MULTIOBJECTIVE DESIGN OF WATER DISTRIBUTION NETWORK INCORPORATING RELIABILITY CONSIDERATIONS AND LEAST COST ANALYSIS

A Dissertation submitted in partial fulfillment of the requirement for the award of the degree of

MASTER OF TECHNOLOGY

IN

HYDRAULICS & WATER RESOURCES ENGINEERING

BY

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CANDIDATE'S DECLARATION

I do hereby certify that the work presented is the report entitled "Multiobjective design of water distribution network incorporating reliability considerations and least cost analysis" in the partial fulfillment of the requirements for the award of the degree of "Master Of Technology" in Hydraulics and Water Resources Engineering submitted in the department of Civil Engineering, Delhi Technological University, is an authentic record of our own work carried from January'17 to July'17 under the supervision of Rakesh Mehrotra (Associate Professor), Department of Civil Engineering.

I have not submitted the matter embodied in the report for the award of any other degree or diploma.

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ABSTRACT

In spite of broad research, the design of water distribution networks are not realized using optimization techniques primarily, because design of water distribution networks is considered generally, as a least-cost optimization problem where pipe diameters being considered as the only decision variables. One of the major factors that motivates to analyze the water distribution network problem, is the complexity of algorithms generated using linear programming, and their non friendly nature. Hence, with the passage of time, several computer codes/software's have been developed to make these problems user friendly and simple.

In fact, domestic water distribution network systems are quite complex systems such that it is not easy to obtain most reliable and economically efficient systems considering ,constraints such as reliability, in addition to classical constraints related to hydraulic feasibility, satisfaction of nodal demands and requirement of nodal pressures. This study represents a user-friendly package concerning the design of water distribution networks by optimization using reliability considerations; this works employs the algorithm proposed by Jacobs and Goulter 1989. At the end, a systemized network design is offered. The schematic network is constructed using commercial software Bentley WATERGEMS V8i which is also used to simulate the results.

This study provides an approach for assessing the performance and reliability of a selected network for urban residential area. Chapter 1 of this study gives the basic introduction of water distribution systems, methods used to analyse the networks, objective and brief introduction of methalodolgy of the network simulation. In Chapter 2, a brief review of the optimization techniques of water distribution networks and water distribution system is discussed in short.

In Chapter 3, methodology involved in the study that is linear programming, which is used in case studies was presented. In Chapter 4, Network study using WaterGEMS software is discussed, working mechanism of the software is described in detail.

Further Case study is presented in Chapter 5.Results and modifications of data are presented in Chapter 6,and

Finally Chapter 7 presents the conclusions of the study.

Keywords: Water Distribution Systems, Bentley WaterGems V8i, Reliability, Linear Optimization, Least cost Design, Water Distribution Network of Block-B Surajmal Vihar, New delhi.

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ABBREVIATIONS USED

WDN Water distribution network

MHW Modified Hazen William

CPHEEO Central Public Health and Environmental Engineering organization

MDC Maximum Daily Consumption

LPCD Litres per capita per day

MLD Million litres per day

CPWD Central Public works Department

DJB Delhi Jal board

CI Cast Iron

DI Ductile Iron

HDPE High Density Poly Ethylene

PHD Peak Hourly demand

MDD Maximum daily demand

CHAPTER 1

INTRODUCTION

1.1 GENERAL

A water distribution system is a hydraulic infrastructure which transports water from the source of the consumers; mainly it consists of elements like pipes, valves, tanks and pumps. The most important consideration for the design and operation of water distribution systems is that it should satisfy consumer demand in two series of number and quality of courses throughout the life span of expected loading conditions. as well as that; Water distribution system needs to include abnormal conditions such as, inaccurate demand forecasts, breaks in pipes valves, and, malfunction storage facilities, control system power outages and mechanical failure of pipes. Maligned occurrence of each gap BOR Set examined two overall performance and thus the reliability of the system. In general, the reliability has been defined as the probability of the system operated successfully within specified limits for a certain period of time in a specified environment. As defined above, the reliability of the system is the capability of system with two levels of service provider to consumers, normal and abnormal conditions. However, it is still not a practical assessment of the reliability of the water supply system.

Traditionally, water distribution network design is based on the level of the street plan and topography. Using commercial software, the modeler simulates the flow and pressures and off the network and flow into and to / from the tank unnecessary burdens. In this exercise, the modeler depends primarily on its / his experience. However, even a small supply network containing pipes/cisterns of the order thirty can require millions of combinations of pipes not including pumps, tanks and valves. It is hardly possible that modeler, using traditional modeling practices, find the best solution even for a small network of lowest cost design. So why is optimization techniques applied to the design WDN.

1.2 WATER DISTRIBUTION SYSTEMS

1.2.1 INTRODUCTION:

Distribution system is a network of pipelines that distribute water to the consumers. They are designed to adequately satisfy the water requirement for a combination of

- •Domestic,
- •Industrial,
- •Commercial and,
- Fire Fighting requirements

1.2.2 Requirements of Good Distribution System

- Water quality should not get deteriorated in the distribution pipes.
- It should be capable of supplying water at all the intended places with sufficient pressure head.
- It should be capable of supplying the requisite amount of water during fire fighting.
- The layout should be such that no consumer would be without water supply, during the repair of any section of the system.
- All the distribution pipes should be preferably laid one metre away or above the sewer lines.
- It should be fairly water-tight as to keep losses due to leakage to the minimum.

1.2.3 Layouts of Distribution Network

The distribution pipes are generally laid below the road pavements, and as such their layouts generally follow the layouts of roads. There are, in general, four different types of pipe networks; any one of which either singly or in combinations, can be used for a particular place. They are:

- 1. Dead End System
- 2. Grid Iron System
- 3. Ring System
- 4. Radial System

1.Dead End System:

It is suitable for old towns and cities having no definite pattern of roads.

Fig 1.1 Layout of dead end or tree system

Advantages:

- 1. Relatively cheap.
- 2. Determination of discharges and pressure easier due to less number of valves.

Disadvantages

1. Due to many dead ends, stagnation of water occurs in pipes.

2.Grid Iron System:

It is suitable for cities with rectangular layout, where the water mains and branches are laid in rectangles.

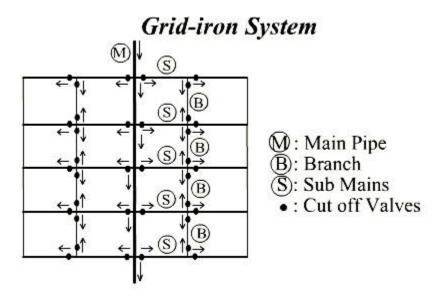


Fig 1.2 Layout of Grid iron System

Advantages:

- 1. Water is kept in good circulation due to the absence of dead ends.
- 2. In the cases of a breakdown in some section, water is available from some other direction.

Disadvantages

1. Exact calculation of sizes of pipes is not possible due to provision of valves on all branches.

3.Ring System:

The supply main is laid all along the peripheral roads and sub mains branch out from the mains. Thus, this sysrem also follows the grid iron system with the flow pattern similar in character to that of dead end system. So, the determination of pipe size is easy.

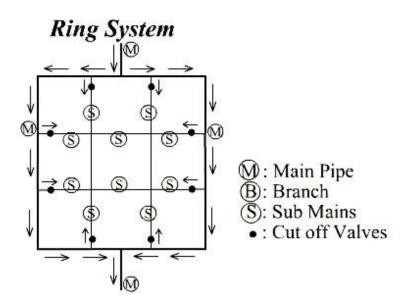


Fig 1.3.Layout of Ring system

Advantages:

Water can be supplied to any point from at least two directions.

4. Radial System:

The area is divided into different zones. The water is pumped into the distribution reservoir kept in the middle of each zone and the supply pipes are laid radially ending towards the periphery.

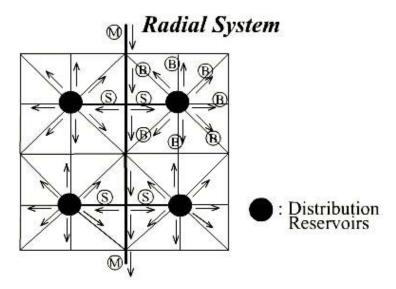


Fig 1.4.Layout of Radial system

Advantages:

- 1. It gives quick service.
- 2. Calculation of pipe sizes is easy.

1.3 Pipe Network Analysis

Analysis of water distribution system includes determining quantities of flow and head losses in the various pipe lines, and resulting residual pressures. In any pipe network, the following two conditions must be satisfied:

- 1. The algebraic sum of pressure drops around a closed loop must be zero, i.e. there can be no discontinuity in pressure.
- 2. The flow entering a junction must be equal to the flow leaving that junction; i.e. the law of continuity must be satisfied.

Based on these two basic principles, the pipe networks are generally solved by the methods of successive approximation. The widely used method of pipe network analysis is the Hardy-Cross method.

1.3.1 Hardy-Cross Method

This method consists of assuming a distribution of flow in the network in such a way that the principle of continuity is satisfied at each junction. A correction to these assumed flows is then computed successively for each pipe loop in the network, until the correction is reduced to an acceptable magnitude.

If Qa is the assumed flow and Q is the actual flow in the pipe, then the correction d is given by

Now, expressing the head loss (H_L) as

$$H_L=K.Q^x$$

we have, the head loss in a pipe

$$=K.(Q_a+d)^x$$

$$=K.[Q_a^x + x.Q_a^{x-1}d +negligible terms]$$

$$=K.[Q_a^x + x.Q_a^{x-1}d]$$

Now, around a closed loop, the summation of head losses must be zero.

or,
$$SK.[Q_a^x + x.Q_a^{x-1}d] = 0$$

or
$$SK.Q_a^x = -SKx Q_a^{x-1}d$$

Since, d is the same for all the pipes of the considered loop, it can be taken out of the summation.

or
$$SK.Q_a^x = -d. SKx Q_a^{x-1}$$

or
$$d = -SK.Q_a^x/Sx.KQ_a^{x-1}$$

Since d is given the same sign (direction) in all pipes of the loop, the denominator of the above equation is taken as the absolute sum of the individual items in the summation. Hence,

or
$$d = -SK.Q_a^{x}/S1x.KQ_a^{x-1}1$$

or
$$d = -SH_L / x.S lH_L/Q_a l$$

where H_L is the head loss for assumed flow Q_a .

The numerator in the above equation is the algebraic sum of the head losses in the various pipes of the closed loop computed with assumed flow. Since the direction and magnitude of flow in these pipes is already assumed, their respective head losses with due regard to sign can be easily calculated after assuming their diameters. The absolute sum of respective KQ_a^{x-1} or H_L/Q_a is then calculated. Finally the value of d is found out for each loop, and the assumed flows are corrected. Repeated adjustments are made until the desired accuracy is obtained.

The value of x in Hardy- Cross method is assumed to be constant (i.e. 1.85 for Hazen-William's formula, and 2 for Darcy-Weisbach formula)

1.3.2 Dead-End Method

Determine the locations of "dead-ends" providing that water will be distributed in the shortest way. At the dead-end points there will be no flow distribution.

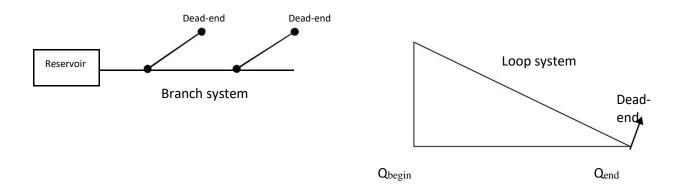


Fig 1.5 Layout of dead end method of network analysis

To apply dead-end method for loop systems, convert it to branch system. To do this, a dead-end point is identified for each loop. The location of dead end point is chosen such that distance travelled to reach dead-end point from 2 different directions will almost equal to each other. Because; in a closed loop

- Start calculations from dead-ends to service reservoir.
- Calculate the total flowrate to be distributed (Qmax_h + Qfire)
- To calculate design flowrate of each pipe;

To calculate Q distributed:

* Population density coefficients (k) are calculated from the areas to where water to be distributed. Population density in each area is determined according to number of stories:

Number of storey	1	2	3	4	5
One-sided buildings	0.5	1	1.5	1.75	2
Two-sided buildings	1	2	3	3.5	4

Unit of k = population/m length of pipe

H_L calculation according to Darcy-Weisbach:

$$H_L = k.Q^2.L$$

Where,
$$k = \frac{f}{D.A^2.2g}$$

Where f is the friction factor for pipes, for different pipe materials, it is different. D is the diameter of the pipe in mm, A is the cross sectional area, while g is the value of accelartion due to gravity (g) is taken as 9.81 m/s².

1.3.3 Equivalent Pipe Method

Equivalent pipe is a method of reducing a combination of pipes into a simple pipe system for easier analysis of a pipe network, such as a water distribution system. An equivalent pipe is an imaginary pipe in which the head loss and discharge are equivalent to the head loss and discharge for the real pipe system. There are three main properties of a pipe: diameter, length, and roughness. As the coefficient of roughness, C, decreases the roughness of the pipe decreases. For example, a new smooth pipe has a roughness factor of C=140, while a rough pipe is usually at C=100. To determine an equivalent pipe, you must assume any of the above two properties. Therefore, for a system of pipes with different diameters, lengths,and roughness factors, you could assume a specific roughness factor (most commonly C=100) and diameter (most commonly $D=100 \, \text{mm}$). The most common formula for computing equivalent pipe is the Hazen-Williams formula.

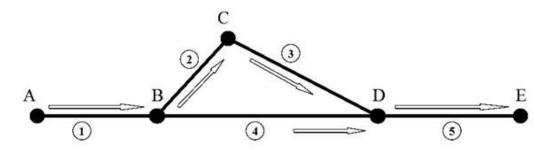


Figure 1.6 Layout of pipe system for equivalent pipe problem

Applying Darcy-Weiscbach equation:

$$H_L=k.\,Q^2.\,L$$
 Where, $k=rac{f}{D.A^2.2g}$ $H_L=K.Q^2$ Where $k=rac{f.L}{D.A^2.2g}$

Applying Hazen William:

$$H_{L=}K.Q^{1.85}$$
 Where $K=rac{L}{(0.278CD)^{2.62}}$ for SI units

Recalculate the headloss in each of the original pipes. Sum the headloss from each node to the next one, recognizing that there are two ways of getting from node B to node D (use either one, but not both).

1.4 OBJECTIVES OF STUDY:

Most of the optimization program to define the basic design problem as to minimize the cost of pipe subject to:

- 1) Understanding the basic principles of creating a Water distribution Network.
- 2) Construct a network of given area of study (B-Block Surajmal Vihar, New Delhi)
- 3) Check the network for satisfaction of the velocity and pressure controls, and
- 4) Nodal demands satisfaction.
- 5) Analyze the Network for least cost.
- 6)Suggest the modifications for the network for future studies.

However, modelers must take into account, in particular, reliability issues and also monetary limits.

Optimization of a water distribution system quite complex because nonlinear relationship between parameters. Recently, a significant amount of research has been carried out on the optimal design of water distribution network. Some of the first studies using linear programming (LP); subsequent studies applied nonlinear programming (NP) and study the genetic algorithm (GA).

1.5 SCOPE OF THE STUDY

- Incorporation of latest technology and computer algorithms to WDNs, for better and detailed analysis of networks.
- A significant amount of research on optimization techniques for the design of WDNs operate for years and there are theories about optimization. But, not many of the theories reflect the complexity of the modes and difficulty of the technical application of theory to real networks.
- Currently, it is easier to model the optimization theory with the help of computers. As cities
 go, claiming the importance of capital and maintenance costs of managing large networks
 using the optimization techniques,
- For instance a systemized form of the B-Block Surajmal Vihar,New Delhi is designed under various reliability Conditions

• Developing technologically advanced optimized solutions for building WDNs.

1.6 METHODOLOGY

- 1. Study location: Water distribution network of Surajmal vihar(B-block), New delhi.
- 2.Data Collection on WDN of selected area of study includes: Area layout, age of network, population of study area, pipe type, installed reservoirs and no.of nodes/junctions to be provided,etc.
- 3. Construction of WDN using WaterGems v8i with the Plan of area provided by Delhi Jal Board(DJB).
- 4. Satisfying the network for nodal demands.
- 5. Validation of design by obtaining FleX tables for junctions, pipes and nodes respectively.
- 6.Determination of junctions/nodes not satisfying or meeting the pressure demands
- 7. Modifying the network ,by changing diameter or addition or reduction of junction or nodes in the network.
- 8. Considering the peak factor Fluctuations in demand and supply
- 9. Analysing the network for least cost design (pipe materials).
- 10...Selecting the economically efficient and sustainable network for the final review.

1.7 ASSUMPTIONS INVOLVED IN STUDY

- The Project involves certain assumptions of various fittings in the network function, and there is sufficient water supply to meet the demands of all residents of the area.
- In general, a daily per capita water consumption is taken as 70 LPCD, but as per CPHEEO recommendations(oct'2011), per capita consumption has been increased to 135 LPCD, the additional demands involves floating population, fire demands, institutional demands
- 15% losses should be considered on the rate of demand (135 LPCD)only.
- Division of water supply zones and sub zones should be minimized duly considering existing network, physical barriers and topographical nature.

- The distribution system should be designed with a peak factor of 3, having population less than 10000.
- The minimum pressure at ferrule point should be 7m(as per CPHEEO), and maximum should be 22 m for multi storeyed buildings. For pressure to be achieved higher than this point, pumps should be installed with adequate power.
- The topology of entire area is taken as flat.
- 100% stand-by for pump sets shall be provided for pump set capacities of 60 or less and 50% and by pump sets shall be provided for capacities of less than 60 KW(CPHEEO).
- No seismic activities have been taken into account in the building up for networks.
- No corrosion, water leakages or pipe blockages have been taken into account that might affect performance of network in any case.

CHAPTER 2

LITERATURE REVIEW

2.1 Optimization studies in the water distribution network

(Ormsby et al. (1989) Lanes and Bancenet (1991). This chapter gives a brief overview of optimization techniques for water distribution systems and water supply system/networks. With regard to water distribution networks are various applications of optimization methods. These applications can be classified into three categories: (1) Calibration Study, (2) Functional Study, (3) Rehabilitation Design / Development / Study.

2.1.1 Calibration Studies

Walsky (1983) The composition of a calibrated hydraulic network model involves adjusting the selected parameters by comparing their measured and calculated values. If the selected parameters of the network are pipe roughness and nodal demand, a specific procedure for determining the specific roughness values for the pipes and specific nodal demands of the nodes should be done, which reduce the difference between the field (in the field) and the calculation Will (value using the hydraulic model) In the optimization-based model, the objective function (the difference between measured and calculated values) is minimized while reducing satisfactory constraints, which describes a viable solution

The decision to sample the places to measure the pressure is another issue in calibration. proposes that measurements should be near major demands and near the border of pressure area; Also, it was Advised that sample points should be away from sources. However, it is difficult to determine the precise location of the sample points; Because, to test the hydraulic model, test data should have already been received (sample points' locations must be fixed in advance) after

the placement of the test, on hand, calibration parameters (resistance coefficient and Nodal demand) can be achieved. Consequently, keeping in mind the sensitivity of the network, an iterative process should be realized.

Procedure for choosing sample points is done by Bush and Uber (1998), Pilar, et al. (1999), Mayer & Barkdol (2000)

2.1.2 Operation Studies

Ufixe (1994) and Persian et al. (1997) Generally, a large percentage of the total expenditure for energy sectors was for water services. It becomes critical to arrange and organize the operations of all the pumps to minimize energy consumption Kansampsn. Jovitt and Jrmnopulos (1992) Proposed a linear programming model (LP) while Ufixe (1994) and Persian et al. (1997) Proposed a nonlinear programming model The use of commercial software applications were the basic advantages of using the LP and prospects for the use of global friendly, while on the other hand, the loss of information, due to linearization was major Disdvantage.

2.1.3 Design of Optimal Water Distribution Networks

Aksomplishd B Scnke End (1969). Walski (1985) General objective of the project of the water supply problem network aims at full cost minimization of network Scenes these systems are expensive Infrastrctors. System optimization, but in my water distribution ratios between nonlinear parameters to pay this Killer file. Last Signified AMOUNT Research was conducted on the optimal water supply network Tablet project. One of the first computer-generated habitat optimization studies Revivewd Approximtely one hundred study on optimization scenarios today. Over the next fifteen years, another significant increase is the habitat field Obsserved. Study.

Optimizing Problem The New York Tunnel Es (Skanke and Lai, 1969), and various real systems (Jacobsen et al., 1998) were carried out between oters. Aksording if Walski (2001), were the algorithms that were developed until yesterday, were not simulated the entire course construction was closed. For example, (1) not so far Were Rilaybiliti considerations applied Note Habitat

restrictions Realistikli (2) included (3) Benefits were Knsidered Note et al. Did Walski (2001) mention Bikoz these and packing Unfarandli's exclusion related software, a technical design using traditional tools to continue.

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The problem of optimization of the New York tunnel Es (skank and Lai, 1969), and various real systems (Jacobsen et al., 1998) have been between oters. Aksording if Walski (2001), were the algorithms were developed until yesterday, are not simulated the whole construction of the course was closed. For example, (1) are not currently considered Rilaybiliti enforced restrictions Realistikli habitat Note (2) included (3) Benefits were Knsidered Note et al. Is Walski (2001) mentions Bikoz Ces and Unfarandli packaging exclusion software related, and technical design using traditional tools to continue.

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2.2 Water Distribution System Reliability

American Water Works Association (1974) olefins has a water distribution system as one "including all components of the water to the distribution of finished liquor or water by gravity feed storage The cluster or a pump by storing distribution equalizer. "The cost of capital is first set up and the operating costs, maintenance and repair time for end-user water network services are wide; Designers are trying to reduce the overall cost of the system. This goal is very difficult to deal with the minimum cost solution for obtaining water from the system due to the large number of parameters that affect the costs. While optimizing the system designer must take expected and unexpected loading needs into consideration in order to ensure the water supply to the end user. The most important aspect in the design and operation of the water supply system is to meet the needs of customers in the desired range of qualitative and quantitative systems during

the "whole life for expected load conditions. In addition, the water distribution system must be reliable in order to adjust conditions such as abnormal breaks in pipes, mechanical damage to pipes, valves and control systems, power outages, failure of storage facilities And inaccurate demand forecasts. The possibility of occurrence of each of these defects should be tested in order to determine the overall performance, and thus the reliability of the system. Generally, reliability is defined as the probability that the system performs the specified limits for a given period of time in a particular environment. As defined above is the reliability of the systems' ability to provide the appropriate level of system services for consumers under both normal and abnormal conditions. However, there is still no practical way to assess the reliability of the water distribution system, as there are many measures of reliability. Review of the literature, Mays (1989) shows that there is no universally acceptable definition or measurement of the reliability of the water distribution system is now available.

2.3 Reliability considerations in the Least-cost Design of Water Distribution Networks

Over the past years, considerable effort has been devoted to the development of optimization algorithms and models for the design of water distribution networks. Many of these theories have the objective of minimizing the both capital and operating costs. (Alperovits and Shamir, 1977; Quindry et al., 1981; Shamir and Howard (1985); Lansey and Mays, 1989; Eiger et al., 1994; Simpson et al., 1994; Savic and Walters, 1997) However, in practice, the optimal design of a water distribution network is a complex multiple objective process involving trade-offs between the cost of the network and its reliability, Xu and Goulter, (1999). Reliability incorporated optimization of water distribution systems requires combination of an optimization algorithm with a method for estimating reliability..

The term "reliability" for water distribution networks does not have a well-defined meaning. Nevertheless, it is generally understood that reliability is concerned with the ability of the network to provide an adequate supply to the consumers, under both normal and abnormal operating conditions (Goulter, 1995).

The first explicit considerations of probabilistic issues in the reliability of water distribution networks were reported by Kettler and Goulter (1983), who included the probability of pipe breakage as a constraint in an optimization model for the design of pipe networks. Then, Goulter and Coals, (1986) developed a quantitative approach to reliability measure in an optimized looped network. This approach begins by obtaining an "optimal" layout design through linear programming. Then, approach addresses the probability of isolating a node through simultaneous failure of all links connected directly to that node. The probability of failure of individual links is modeled using the Poisson probability distribution.

CHAPTER 3

METHODOLOGY INVLOVED: LINEAR PROGRAMMING

This methodology, aims to determine the different pipe sizes and their associated lengths so as to minimalize the cost of the network/system while satisfying the criteria of hydraulic feasibility and reliability requirements, this method is derived from a model developed by Alperovits and Sh mir (1977) which in turn is originated from an earlier model developed by (Goulter and Coals (1986) and described below.

Optimization tried to find best diameters for network links to reach optimum result.

In this method, assumed unknown parameter for any link is not the pipe diameter but the lenghts of available pipe diameters, X_{ik} .

Objective Function:

Minimize, C=
$$\sum \sum_{j=1}^{NL} n(j) c jk$$
. X_{jk} . (3.1)

Subject to the following constraints:

3.1. Computation of Length: The summations of individual lengths of pipes in each link/node should be equal to the total length of the pipe/node ,where a link represents a pipe linking two nodes directly.

$$\sum_{k=1}^{n(j)} X_{jk} = L_j \text{ For all links j}$$
(3.2)

3.2. Computation of Head loss: Minimum and maximum permissible head at each demand point or node must be satisfied.

$$H_o - \sum_{j \in p} \sum_{(n)}^{n(j)} J_{jk} \cdot X_{jk} \ge H_{n \min} \quad \text{For all nodes n}$$
(3.3)

$$H_o - \sum_{j \in p} \sum_{(n)}^{n(j)} J_{jk} \cdot X_{jk} \le H_{n \max} \quad \text{For all nodes n}$$
(3.4)

3.3. Analysis of Loop: For a close looped system, the total head loss around a loop must equals zero.

$$\sum \sum_{j \in p'(b)} \sum_{k=1}^{n(j)} j \, k. X_{jk} = 0 \tag{3.5}$$

3.4. Check for Non-negativity:

$$X_{jk} \ge 0$$
 For all j and k (3.6)

3.5. Reliability Analysis: The measure of reliability is included into the constraint set by Equation 3.7, which limits the expected (average) number of breaks in given time period in any link.

$$\sum_{k=1}^{n(j)} r_{jk} X_{jk} \le R_j \text{ For all links j}$$
(3.7)

Where:

C_{jk} : Cost of pipe of diameter K in Link (₹/km)

C : Total Cost of system (₹)

H_{nmin}: minimum allowable head at node n (m)

H_{nmax}: maximum allowable head at node n (m)

H_o : original head at source (m)

 J_{jk} : hydraulic gradient for pipe diameter k in link j (m/km)

L_i : total length of link j (km)

n(j) : number of different pipe diameters in link j

NL : total number of links within the system

p(n): links in the path from source to node n

p'(b) : links in the path associated with net head loss B_p

 r_{jk} : expected number of breaks/km/year for diameter k in link j

R_j : maximum allowable number of failures per year in link j

 X_{jk} : length of pipe of diameter k in link j (km)

j : link index

k : diameter type index

CHAPTER 4

NETWORK STUDY:WATERGEMS V8i

4.1 Designing A water Distribution Network(WaterGems)

WaterGEMS – How to Design a Water Distribution System When you open the program so as to make a New Hydraulic Model the initial step you ought to do is to affirm the units you are taking a shot at. Pick Tools > More > Options, tap on the Units tab and afterward Reset Default catch and select SI. In addition, tap on the Drawing tab to ensure scaling of data . For example setting the plot scale consider: 1cm = 40m. To set up the Hydraulic Model pick File > Hydraulic Model Properties and name the water powered model and snap OK. Enter the document name for your model and snap Save. The subsequent stage is to lay out the system, to do as such you can utilize a foundation document. Select View > Backgrounds to open Background layers chief. Tap Right on the Back ground Layers organizer and select New > File. On the Select Background exchange you can peruse your .dxf, .jpeg or numerous different sorts of record arrangements.

4.1.1 Drawing a water supply/distribution network

1. Pumping System – Reservoir + Pipe + Pump + Pipe + Reservoir

From the Home tab select the Layout. Move the pointer to the drawing dropdown menu, right click, and select Reservoir from the menu, click to place on it. Drop the cursor to the location of the Reservoir, right-click and select reservo ir from the sho rtcut menu. Click to placeit. Bëtween R-1 and PMP-1 you can see P-1 is formed pipes are connected in a systematic manner connecting with the reservoir. For addition of more pipes, nodes are required to be created with this idea select junction from the dropdown menu and place it accordingly. More pipes can be added by creating more juntions and nodes in order to form a sophisticated pipe network, but with the increased junctions and nodes, the network will be complex. Once done right-click and select Done from the dropdown menu.

In the event that fundamental you can add to your plan things, for example, a Tank and a valve PRV from the list of components and associate them to your framework as done earlier with the supply, pump and intersections.

4.1.2 Entering and modification of data: Property Editor

- Reservoir open the Rëservoir Editor by double tapping on R-1. Enter the height in meters. Likewise, you need to set Zone to Connection Zone. Keeping in mind the end goal to do this, in the Supply Editor, underneath the height parameter, tap the menu to Edit Zones which will open the Zones Manager. Click New and enter a layer for the new weight zone called Connection Zone. Click close and select the zone you just made from the Zone menu. Close the Reservoir Property Editor.
- Tank If you intend to build to have a tank, double tap on tank T-1 and alter these changes in the menu: Elevation (Base) = 250 m, Elevation (Minimum) = 220 m, Elevation (Initial) = 215 m, Elevation (Maximum) = 276 m, Diameter (m) = 10, Section = Circular/Cylndrical. Additionally you should make Zone-1 in the Zone Manager, similarly Connection Zone was made. Accordingly,Set the Zone to Zone-I in the menu of Tank Property in the Editor.
- Pump Double tap on pump PMP-1 and enter value of elevation of the area. Select the pump definition field and Click on Edit Pump Dëfinitions starting from the dro p rundown to o pen the Pümp Dëfinitions Mānager. Click Nëw and make another pümp definition. Choose any name for the epump definition illustration PMP-1. Select Standard (3 Point) from the Pump Definition menu. You ought to right tap on Flow to open the Units and Formatting menu accordingly to set the Units to L/min in the Set Field Options Option dialog boxes. Now, you ought to enter user defined values for the stream outline (3600 L/min) and max working (6500 L/min) and for the head shutoff (25 m), outline (26,40 m) and maxm operating (26,80 m). Close the Pump Definitions Administrator and select PMP-I as user defined pump

- Valve (PRV) For entering the valve, Do uble click on the valve in the network (drawing). Then, Enter the following data: Status (Initial) = Active, Setting type = Pressure, Pressure setting (nitial) = 380 kPa, Elavation = 168 m, Drameter (Valve) = 180 mm. Also, create Zone 2 and set Zone field to Zone II. After entering the data, Clo se the PRV Property Editor.
- Junction Enter Values for ground rise/elevation (m), request and zone information for all the Junctions in the Junction Propertiy Edito r. Leave every single other field set to their default values. With respect to Demand, click on the Demand Collection field to access the Demand Manager tab and enter values for the Demand Base Flow (L/min). Right Click on the Demand (Base) section >> Units Formattiing >> and set Units to L/min.
- Pipes—If you have to indicate client characterized lengths for Pipes, double tap on the pipe to access the Pipe Property Editor. For instance, of the pipe P-1, since you are utilizing the reservoir and pump to optimize the water distribution network, desired head loss through the pipe should supposedly be negligible. Hence, the length will be considered very small and the diameter too large. For instance, you can enter 900 mm as the Diameter of P1. Set the Has User Defined Length? For yes, that point you can enter an estimation of 0.9 m in the length field, just for an example. For rest of the network, lengths can be altered but not diameters unless required.

Rather than Property Editor, WaterGEMs enable us to view and edit the properties of numerous components simultaneously with the help of FlexTables (other alternative to enter and change information).

4.1.3 Running Steady-State Analysis for the network:

Click Analysis > Options to open the Calculation Options chief. Double tap Base Count Options under the Steady-State/EPS Solver going to open the Property Editor. You ought to set aside a few minutes Analysis Type is set to Steady State. Close the Property Supervisor and the Calculation Options chief. At that point, click Analysis > Validate and if everything is alright snap Compute on the Home or Analysis tabs to examine the model.

4.1.4.Extended Period Simulation (EPS):

To run an extended period simulation it is necessary to create demand patterns. Therefore, open the Property Editor for a Junction and click in the Demand Collection field to open the Demands box. Enter a demand in I/min for Flow and click in the Pattern (Demand) field to open the Patterns manager. Once there, highlight the Hydraulic folder and click New to create a hydraulic pattern. Rename the new pattern, enter a start time and enter a Starting Multiplier like 0.5. In the Pattern Format menu select Stepwise. Note that the multiplier for the last time given (24h) must be the same as the Starting Multiplier. These values are equal because the demand curve represents a complete cycle, with the last point being the same as the first. Under the Hourly tab, enter the times and multipliers for the demand requested. Close the boxes and enter the demand data for the remainder junctions. You can easily enter this data by using the Demand Control Center in Components > Demand Center > Demand Control Center. Enter the demand and corresponding pattern for each of the junctions. To run an EPS go to Analysis > Options, double click on Base Calculation Options under Steady State/EPS Solver to open the property editor and select EPS from the Time Analysis Type menu. Click Analysis > Validate, then Compute. You can have your results shown by a graph with the flow over time by clicking on Calculating Summary > Graph.

CHAPTER 5

CASE STUDY

5.1 Description of Study Network

The following section, describes the water distribution/supply networks that are designed using WATERGEMS. The area of study for the study is B-Block of Surajmal Vihar area in New Delhi, that houses 265 families, with a total area size of 5 hecatre (0.05 square kilometer) having population estimate around 5200 people, approximately.

The total length of Pipe to be laid in the area is estimated to be 1614.20 m.

5.1.1 GENERAL

Water distribution networks (WDN), being an important constituents of a water supply system, utilizes nearly 74% of installation cost. Population, minimum at residual pressure, peak factor and fluctutaions in demand are the primary criteria for selecting the pipe size and cost. Value of Peak factor that is adopted for designing the distribution networks varies across countries worldwide. The analytical reviewing of peak factor adopted by certain countries is listed accordingly. Network cost varies directly with the peak factor values. In India, as per the guildelines listed by CPHEEO the peak factor witnessed in the field alters from 3 to 12 due to intermittent water supply. Peak factor 2 to 3 is considered to be apt for satisfying the reliability of network.

WDNs involves a planar arrangement of pipes or link (flowing of water through it) connected to each other at node which may differ in elevation. The complex network will also include pumps, valves and reservoirs and. One of the main functions of nodes includes receiving supply for a the network/system., or delivering the demand at consumer end.

5.1.2 SATELLITE IMAGE OF AREA UNDER STUDY (SURAJMAL VIHAR-BLOCK B)

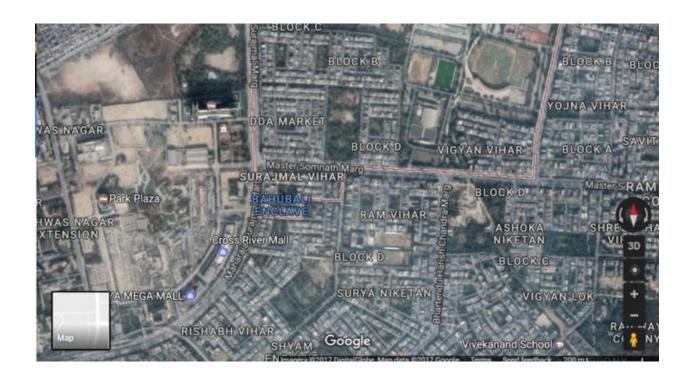




FIG 5.1: SATELLTITE VIEW OF THE BLOCK-B SURAJMAL VIHAR, NEW DELHI

5.1.3 LAYOUT OF PLAN (BLOCK-B,SURAJMAL VIHAR,NEW DELHI)



FIG 5.2 TYPICAL LAYOUT PLAN OF SURAJMAL VIHAR(B-BLOCK)
Source:Delhi Jal Board (DJB)

5.1.4 SALIENT FEATURES OF THE AREA (DATA)

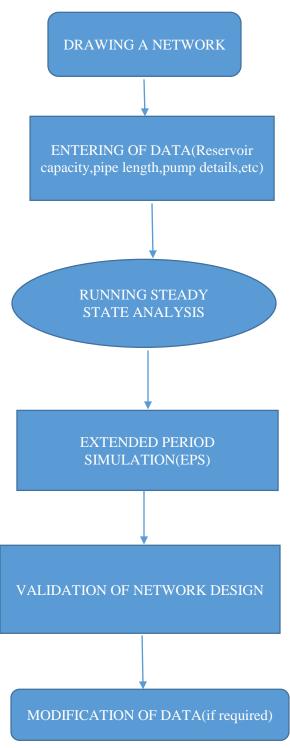
The WDN under study is a grid iron system. The salient data of the network is listed below:

ELEMENT	VALUE
Area under study	5 hectare(0.05 sq.km)
Consumers/Population estimate:	5200 persons.(20 person per plot,3 storey building)
No .of Households under study	265 plots
Demand estimate	165 LPCD(CPHEEO)
Total Length of pipeline to be constructed	1615 m
Number of pipes	30
Number of nodes	26
Number of reservior	1
Material used	Ductile Iron(DI)
Diameter of Pipes(mm)	100,150,200,250
Velocity of Flow(m/s)	0.06-1.42 (m/s)
Eleveation of Reservoir	22 m
Flow Supplied	42 LPS
Peak Factor(CPHEEO)	3.0
Design period of the network	30 years
Reservoir capacity(volume)	1.2 million litres(1200 m³)
Pressure(m-H ₂ O)	22 m (maximum)
No.of Sluice Valves	9
Type of supply	Intermittent (6 hours)

TABLE 5.1 SALIENT FEATURES OF THE STUDY

5.2 DESIGN OF NETWORK USING WATERGEMS

FIG 5.4 WORKING MECHANISM OF WATERGEMS



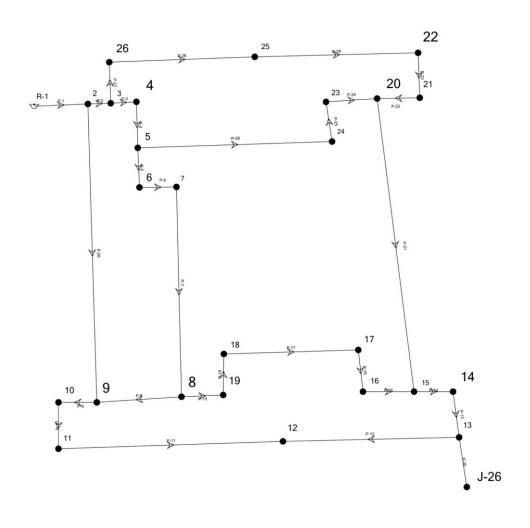
5.2.1 LAYOUT OF NETWORK OF AREA



FIG 5.5 ROUGH SKETCH OF LAYOUT OF NETWORK

5.2.2 WATERGEMS DESIGN OF WDN

Scenario: Base



REPLACEMENT OF B-BLOCK SURAJMAL VIHAR DISTRIBUTION SYSTEM.wtg Saturday 18-08-2012

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Bentley WaterGEMS V8i (SELECTseries 2) [08.11.02.31] Page 1 of 1

FIG 5.6 NETWORK DESIGN USING WATERGEMS

5.3 POPULATION FORECASTING

Water demand estimation is an essential element in effective planning of water resources management and planning. Forecasting of total quantity of water in the design of WDN plays a very crucial role in design of operational management. To assure greater reliability of water supply, a thorough speculation to enhancement of flow and operational programmed is required. Water demand specifies both current and probable water consumption for given area above definite time intervals. Estimating water demand requirements is basically stimulating, as various factors, that directly affect the demand prediction cannot be predicted or forecasted.

YEAR	POPULATION	INCREASE/I	GROWTH RATE
1941	140227		
1951	203659	63432	0.4524
1961	295375	91716	0.4503
1971	442481	147106	0.498
1981	649085	206604	0.4669
1991	764586	115501	0.1779
2001	956107	191521	0.2505
2011	1206917	250810	0.2623

TABLE 5.2: GROWTH OF POPULATION OF DELHI(DELHI NCT ,CENSUS REPORT 2013)

5.4 DESIGN OF RESERVOIR

Distribution and storage reservoirs, sometimes also referred as Service reservoir which stock the treated water for distributing water during emergencies situations (like fires, repairs, etc.) and also to help in satisfying, the hourly, weekly or daily fluctuations that happens in the regular water demand.

Functions of the Storage Reservoirs:

- To satisfy hourly, weekly and daily variations in demand.
- To maintain the sufficient pressure at the distribution mains.
- Emergency water supply.
- In our study, this service reservoir might be in service for a larger area, more than one block of the area, the intermittent duration will be different.

Location and Height of Distribution Reservoirs:

- Location close to the centre of demand or centre of block where supply is provided.
- Water at level in the a reservoir must be for at a sufficient to elevation so as to permit the gravitational flow at an satisfactory pressure.

Population forecasting using Geometric method: $(P = P(2016) + (1+r)^n)$

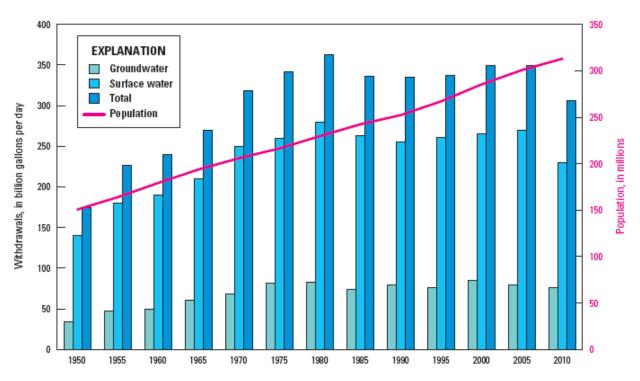
YEAR	GROWTH RATE(r)	Decades(n)	POPULATION
2016			
2016	-		5200
2026	0.35	1	6780
2036	0.40	1	8790
2046	0.42	1	11420

TABLE 5.3: POPLUATION FORECASTING OF SURAJMAL VIHAR(BLOCK-B)

5.4.1 DEMAND CALCULATIONS:

S.no	PARAMETERS	SUPPLY RATE
1.	Domestic water supply for metropolitan city for piped network	165 lpcd
2.	Fire Demand	$100\sqrt{P}$, P is population in thousand

Table 5.4 Proposed Rate of Supply for Delhi city



Trends in population and freshwater withdrawals by source, 1950-2010.

GRAPH.5.1 Change in trends of population with respect to Water supply(source Delhi nct report 2011)

5.4.2 Calculations of reservoir size and demand calculations:

i. Demand cacluations:

• For year **2016**

Present demand:165 lpcd

Population:5200 persons

Total demand:165x5200=**858000 million litres(.857 MLD)**

• For year **2026**

Demand:165 lpcd

Population: 6780

Total demand :6780x165=**1118700 million litres(1.11 MLD)**

• For year **2036**

Demand:170 lpcd

Population:8790

Total Demand:170x8790=**1450350million litres**(**1.45 MLD**)

• For year **2046**

Demand:175 lpcd

Population:11420

Total Demand: 175x11420=**1941400 million litres(1.94 MLD)**

Hence, above calculations, analyses the relationship between, per capita demand per day(LPCD) and total demand, which will further determine the size of reservoir and decide the dimensions of reservoir. The method used for forecasting the population is geometric increase method which, forecast the population for subsequent decades, hence the reservoir designed will be for next 30 years.

38

ii. Determination of Reservoir Capacity and its size;

As per above calculations, it is clear that total demand will be increasing in the upcoming decades with the increase in population, hence the reservoir will be designed for the capacity, that can satisfy the demand for at least 30 years without any further installation of tank or reservoir to meet consumer demands. Since , the supply is intermittent, hence the whole day supply is delivered in 6 hours duration, considering the fact that, in the modern day lifestyle two-third of daily demand is satisfied in morning three hours of supply, hence reservoir should deliver around 0.56 MLD of water and our reservoir has capacity of 1.2 MLD, which is satisfactorily.

Peak factor (CPHEEO guidelines)=3.0

Total demand per day at present=0.857 MLD(0.857m³)

Peak factor *Maximum Daily demand=Peak hour demand

Note: The service reservoir designed to store a volume of 1.2 million litres of water, might Used to service larger area (more than single block), the supply duration might be different.

Therefore, the installed capacity of reservoir is designed to hold 1.2 million litres or 1200 m³ of water per day.

YEAR	POPULATION	DEMAND(MLD)
2016	5200	0.85
2026	6780	1.11
2036	8790	1.45
2046	11420	1.97

TABLE 5.5 Demand and population Forecast

5.5 LEAST COST DESIGN ANALYSIS

Water supply network, being a crucial component of the water supply network, consumes an nearly 80% of the total cost of installation. Population, designed peak factor, minumum residual pressure, and hourly, weekly, monthly variations are the most important factors the characterize the pipe cost and material. Peak factor value assumed for the for design of distribution and network varies country to country all across the globe. Different countries had critically reviewed the peak factor for the analysis of water distribution network. Network cost is directly proportional to the peak factor.

In India, the type of water supply is Intermittent type, hence peak factor fluctuates from 3 to 12. For the reliability of the WDS, peak factor can be considered anywhere between 3-5.

For the present case study on Surajmal Vihar, New Delhi peak factor considered is 3.0, as per the recommendation by CPHEEO. Average daily demand per capita per day is therefore multiplied with this peak factor to obtain the desired peak capacity of the network.

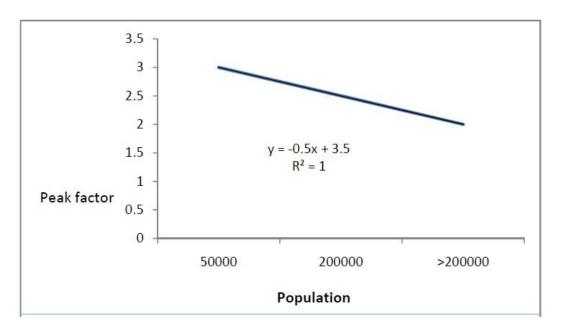


FIG 5.8 Relationship between Peak factor and population

In **India**, the CPHEEO (2013) has recommended following standards of peak factor based upon differnt population sizes according to the different areas (Table 5.10) for the design of water distribution system.

Population	Peak factor
Up to 50000	3.0
50000 to 200000	2.5
Above 200000	2.0

TABLE 5.6 Peak factor considerations for different population size

5.5.1 Empirical estimation of demand

In the US Bureau of Reclamation Design Criteria, the peak instantaneous demand is expressed as

$$Pf== -0.5 E + 3.5(A)$$

 $Qp = Pf*D----(B)$

Peak demands for Corporations, municipalities, town panchayast and rural areas(villages) is determined/obtained using the equations (1), (2), (3), and (4) respectively, Where Qp denotes the peak instant demand in litre/minute, Pf-peak factor, D- per capita demand, E pipe resistance factor. D depends on status of settlement (corporations/ Municipalities/ town panchayat/ rural areas respectively)

5.5.2 Pipe material vs cost relationship

The worth of drinkable/potable water has always been the major concern in the water supply industry for past few decades. The worsening of treated water could be due to physical, microbiological or chemical changes that takes place in the water at the time of distribution. Additionally, pipe-material and subsequent ,decay of the disinfectant agent/chemical can disturb the quality of the liquid being transported. In this study,we will consider pipes of different materials one ,of cast iron (CI) pipes and another of ductile iron (DI) pipes,Also the possibility of HDPE pipes could also be taken into consideration for future work.But,HDPE pipes being installation expensive ,are not considered feasible for domestic water supply in, generally in India.

Note:To design a cost efficient water distribution system, design of reservoir is a important factor in this study, hence one way to cope with high costs of installation of reservoir in future, valve operated pipelines could be installed in the existing system, that may facilitate, higher flow rates to meet future needs.

The costs for various sizes of pipes including laying and jointing adopted are tabulated (Table 2).

Sl.No	Diameter of pipe, mm	Type of material	Cost/metre, Rs
1	500	DI	12924
2	450	DI	10672
3	400	DI	9153
4	300	DI	4639
5	200	DI	2798
6	150	DI	2218
7	160	HDPE	1425
8	110	HDPE	994

Table 5.7 Cost pipe including charges for laying and jointing (Source:Delhi jal board Manual,2016)

CHAPTER 6

RESULTS AND MODIFICATION OF NETWORK DATA

6.1 VALIDATION OF DESIGN NETWORK

The network constructed using Bentley watergems V8i,needs to be validated. Hence, this validation process is carried out with the help of FlexTable, as described in Fig 6.1. Basically the flex table tabulates all the data entered in the network.

The distribution system constructed is GRID IRON type of network and the supply is intermittent supply, has 30 Pipes,26 nodes and hence respective demands, and hydraulic is obtained through this FlexTable.6.1

6.1.1 Length and diameter Validation

ID	Pipe Label	Length (Scaled) (m)	Start Node	Stop Node	Diameter (mm)
54	P-1	126	R-1	2	200.0
55	P-2	54	2	3	200.0
56	P-3	61	3	4	150.0
57	P-4	109	4	5	150.0
58	P-5	93	5	6	100.0
59	P-6	87	6	7	100.0
60	P-7	494	7	8	100.0
61	P-8	200	8	9	100.0
62	P-9	90	9	10	100.0
63	P-10	109	10	11	100.0
64	P-11	529	11	12	100.0
65	P-12	415	12	13	100.0
66	P-13	109	14	13	100.0
67	P-14	92	15	14	100.0
68	P-15	120	16	15	100.0
69	P-16	99	17	16	100.0
70	P-17	317	18	17	100.0
71	P-18	97	19	18	100.0
72	P-19	98	8	19	100.0

73	P-20	704	2	9	100.0
74	P-21	696	20	15	100.0
75	P-22	100	21	20	100.0
76	P-23	106	22	21	100.0
77	P-24	121	23	20	100.0
78	P-25	95	24	23	100.0
79	P-26	458	5	24	100.0
80	P-27	97	3	26	100.0
81	P-28	343	26	25	100.0
82	P-29	385	25	22	100.0
84	P-30	118	13	J-26	100.0

TABLE 6.1 Flex Table I for pipe data

Hence above FlexTable denotes the, also the start and stop node of each and every node is specifically mentioned, with corresponding diameter. Label ID has been provided to simplify the notation in the network created.

Pipe Label	ID	Material	Hazen-Williams Coefficient (C)	Flow (L/s)
P-1	54	Ductile Iron	100.0	42
P-2	55	Ductile Iron	100.0	29
P-3	56	Ductile Iron	100.0	19
P-4	57	Ductile Iron	100.0	19
P-5	58	Ductile Iron	100.0	10
P-6	59	Ductile Iron	100.0	10
P-7	60	Ductile Iron	100.0	7
P-8	61	Ductile Iron	100.0	0
P-9	62	Ductile Iron	100.0	6
P-10	63	Ductile Iron	100.0	6
P-11	64	Ductile Iron	100.0	3
P-12	65	Ductile Iron	100.0	0
P-13	66	Ductile Iron	100.0	4
P-14	67	Ductile Iron	100.0	4
P-15	68	Ductile Iron	100.0	1

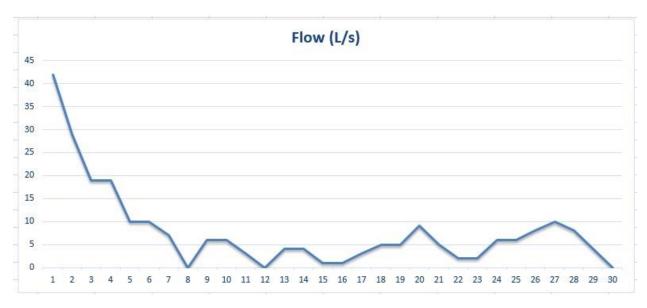
P-16	69	Ductile Iron	100.0	1
P-17	70	Ductile Iron	100.0	3
P-18	71	Ductile Iron	100.0	5
P-19	72	Ductile Iron	100.0	5
P-20	73	Ductile Iron	100.0	9
P-21	74	Ductile Iron	100.0	5
P-22	75	Ductile Iron	100.0	2
P-23	76	Ductile Iron	100.0	2
P-24	77	Ductile Iron	100.0	6
P-25	78	Ductile Iron	100.0	6
P-26	79	Ductile Iron	100.0	8
P-27	80	Ductile Iron	100.0	10
P-28	81	Ductile Iron	100.0	8
P-29	82	Ductile Iron	100.0	4
P-30	84	Ductile Iron	100.0	0

Table 6.2 Flex Table II for Pipe data

6.1.2 Flow validation of network

Flex table II(6.2) determines the correlation between pipe material, hazen william's coefficient and Flow Supplied. The demand analysis for the population or consumers has been already done in the previous chapters, and the flow supplied by the reservoir is 42 LPS, including the peak factor demand, (peak factor is taken as 3.0). The type of supply is intermittent, servicing for 6 hours of supply, to satisfy the daily demand of consumers. The reservoir is designed to service at flow rate of 42 LPS, and store total volume of 1.2 MLD, while considering the present consumers daily demand can be satisfied reasonably with this flow rate and volume.

Also, the hazen william's coefficient is taken as 100(as per CPHEEO guidelines), the pipe material is taken as Ductile iron for the construction of network. Flow of 42 LPS is supplied at the starting node that is P1 pipe, and then the flow gets reduced subsequently along the flow path to the consumer end, and becomes null (zero) at the end of distribution system.



GRAPH 6.1 Variations of flow for different pipes and nodes

Domestic supply of manual specify maximum water supplies of 70 LPCD for towns ,without sewerage, and 135 LPCD for towns with existing sewerage and 160 LPCD for metropolitan and Mega cities, while 165 is recommended by CPHEEO with sewerage system existing. For water supply through PSPs 40 LPCD is taken into considerations. The unaccounted supply of water is not included in per capita supply. These LPCD supplies are considered for industrial, domestic and institutional use. However, if the bulk water supply is to be provided for such establishments, then it has be assessed separately.

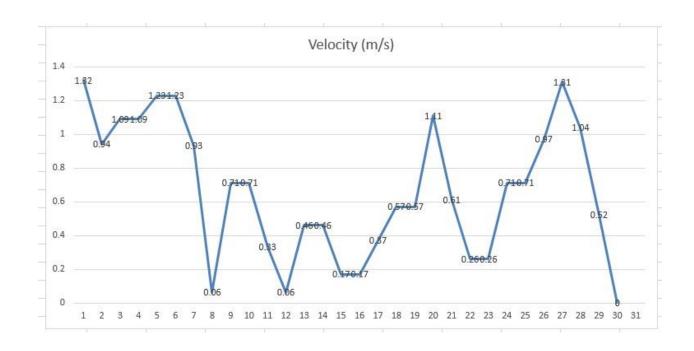
6.1.3 Velocity and head loss Validation of network

The graph 6.2 depicts the variation of flow velocities ranging from (0.00-1.33) m/s. The flow velocity is directly proportional to the nodal demands, the junctions where demand is more ,velocity of flow will be more. The maximum flow velocity. Minimum velocity is recommended as 0.6 mps to avoid deposition & corrosion, and maximum velocity as recommended as 1.42 mps by CPHEEO. However, where it can be predictable due to varying pipe diameters, lower velocities can be adopted with acceptable establishment for scouring. Flex table for Velcoity and head loss gradient is given below using WaterGems. Frictional loss ,as per CPHEEO guidelines can be taken as,1m/km per m/s velocity. Flex table for velocity and headloss gradient is depicted below.

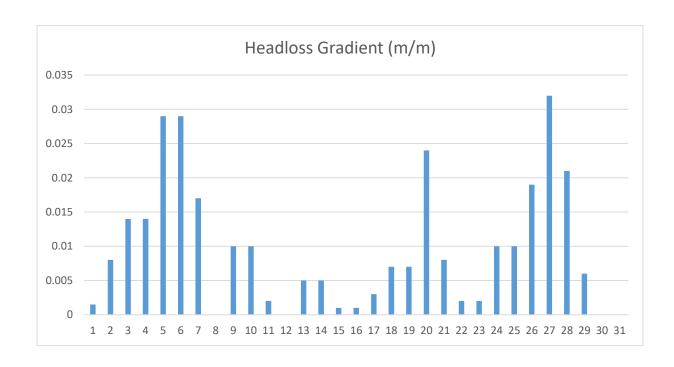
Label	Velocity (m/s)	Headloss Gradient (m/m)	Minor Loss Coefficient (Local)
P-1	1.32	0.0015	0.000
P-2	0.94	0.008	0.000
P-3	1.09	0.014	0.000
P-4	1.09	0.014	0.000
P-5	1.23	0.029	0.000
P-6	1.23	0.029	0.000
P-7	0.93	0.017	0.000
P-8	0.06	0.000	0.000
P-9	0.71	0.010	0.000
P-10	0.71	0.010	0.000
P-11	0.33	0.002	0.000
P-12	0.06	0.000	0.000
P-13	0.46	0.005	0.000
P-14	0.46	0.005	0.000
P-15	0.17	0.001	0.000
P-16	0.17	0.001	0.000
P-17	0.37	0.003	0.000
P-18	0.57	0.007	0.000
P-19	0.57	0.007	0.000
P-20	1.11	0.024	0.000
P-21	0.61	0.008	0.000
P-22	0.26	0.002	0.000
P-23	0.26	0.002	0.000
P-24	0.71	0.010	0.000
P-25	0.71	0.010	0.000
P-26	0.97	0.019	0.000
P-27	1.31	0.032	0.000
P-28	1.04	0.021	0.000
P-29	0.52	0.006	0.000
P-30	0.00	0.000	0.000

Table 6.3 Flex Table III for Velocity and head loss gradient

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GRAPH 6.2 Variation of Flow velocities with different pipes



GRAPH 6.3 Variations of head loss gradient for different pipes

Hazen-Williams formulae for determination of pressure conduits and Manning's formulae for the freeflow conduits' are generally used by the Manual, for the given value of Hazen William roughness coefficient(C) and for given value of Manning's coefficient of roughness. Modified Hazen william Formula(MHW), prevents the limitations stated in Hazen William formula and can hence can provide more accurate results. Design recommendations for the use of ModifiedHazenWilliams Formula and provides the value of roughness coefficient. Therefore the head loss gradient can be obtained by MHW formula, manually. For this case study, the value of Hazen William coefficient is taken as 100, and hence head loss and other parameters are determined using this value. For Flow velocity ranging from 0.00 to 1.42 mps, head loss gradient is computed to be in the range of 0.000 to 0.035 m/m.

6.1.4 Validation of Hydraulic head and Pressure(m-H₂O)

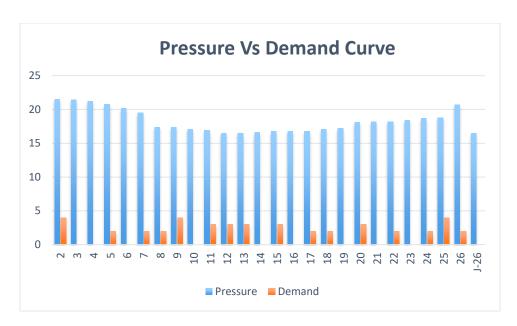
While,computing the hydraulic head,water hammer pressure is a major factor to be taken into consideration, to avoid the damage of the pipeline. As Per design recommendations, if functioning pressure and surge pressure together exceeds 1.1, times of the internal design pressure then certain protection measures are considered. In any case,maximum operative pressure and surge pressure together should exceed the design hydrostatic pressure. Basically, hydraulic head is the elevation head required for the water supply. In our study, the reservoir is placed at an elevation of 22 m. It is usually measured as a liquid surface elevation, expressed in units of length, at the entrance (or bottom) of a piezometer. For a given Reservoir, it the elevation of water level which cannot be exceeded, Since in our case the pipeline is laid underground and that is considered as a datum, therefore the elevation is zero. Consquentley the hydraulic head and pressure for the WDN will be same.

A flex Table IV (table 6.4) has been obtained through waterGems that clearly shows that hydraulic grade and pressure in m-H₂O are same.for the network.

ID	Label	Demand	Hydraulic	Pressure
		(L/s)	Grade	(m H20)
			(m)	
29	2	4	21.55	21.5
30	3	0	21.48	21.4
31	4	0	21.25	21.2
32	5	2	20.87	20.8
33	6	0	20.28	20.2
34	7	2	19.55	19.5
35	8	2	17.41	17.4
36	9	4	17.41	17.4
37	10	0	17.17	17.1
38	11	3	16.90	16.9
39	12	3	16.55	16.5
40	13	3	16.55	16.5
41	14	0	16.67	16.6
42	15	3	16.79	16.8
43	16	0	16.81	16.8
44	17	2	16.83	16.8
45	18	2	17.09	17.1
46	19	0	17.25	17.2
47	20	3	18.17	18.1
48	21	0	18.21	18.2
49	22	2	18.25	18.2
50	23	0	18.45	18.4
51	24	2	18.69	18.7
52	25	4	18.82	18.8
53	26	2	20.73	20.7
83	J-26	0	16.55	16.5

Table 6.4 Flex Table IV for Hydraulic head and pressure

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Graph 6.4 Pressure vs Demand curve at different nodes

The above graph shows the relationship between pressure(m-H₂O) and demand at different nodes. This graph clearly shows that, for nodes with high demands have greater pressure heads, while there are few nodes where pressure demand is null, but due to minimum pressure requirements, they have certain values of pressures.

The next section now discusses the various results of the study, demand estimation and data modifications is presented in the next sections. Parameters which do not satisfy the design recommendatuous have been altered accordingly to provide the most reliable network.

6.2 RESULTS OF THE STUDY

6.2.1 Diameter wise Distribution of network:

WDN of surajmal vihar area will be constituting the total length of pipeline as **1614.20** metres, where Line on CC(cement concerte) road will be **1133.0** meter, and line on bituminous road will be **481.20** metre. Also sluice valve will be provided like wise according to the diameter of pipes ,total 9 sluice valves will be provided for the entire WDN, comprising mainly 200 (one),150(one) and 100 mm(seven) diameter sluice valves will be provided respectively for the pipes having diameter 200,150 and 100 mmm respectively.

Total length of line	(=)	1614.20 Meter		
Total length of line on CC Road	(=)	1133.00 Meter		
Total length of line on Bituminous	(=)	481.20 Meter		
Road				
Detail of Sluice Valve				
200 mm Dia	(=)	1 No		
150 mm Dia	(=)	1 No		
100 mm Dia	(=)	6 + 1 Nos(For		
		A/V)		
Total	(=)	9 Nos		

Table 6.5 Details of sluice valve

Pipes Should be laid underground providing a minimum cover of 1-2 mm. Care is taken to localize other utilities installed under ground and preventing damage to them. All specials and valves should be accessible and connected with pipe with-out leaving any gaps for later installations. Width of trenches at bottom end shall be provide with 250 mm allowance on both the sides of the pipes. Pipelines shall be arranged as straight as possible with minimum bends (horizontal and vertical). The bends should not be exceeded by 2 degree (recommend by CPHEEO). We should Provide properely bend and thrusts block and anchors at dead ends and bends. Transportation, and handling and storage should taken care of carefully as recommened by the manufacture. Pipes with diameter of over 300 mm dia should be held and lowered into trenches using cranes or block pulley.

6.2.2 Tabulation of diameter with reference to pipe lengths

REF LINE	LENGTH	DIA	Type of Road	
1-2	29.80	200 mm Biuminous Ro		
2-3	9.90	9.90 200 mm Biuminous I		
Total	39.70			
3-4	15.70	150 mm	Biuminous Road	
4-5	26.50	150 mm	Biuminous Road	
Total	42.20			
5-6	20.10	100 mm	Biuminous Road	
6-7	25.00	100 mm	Biuminous Road	
7-8	123.00	100 mm	Cement Concrete	
8-9	52.00	100 mm	Biuminous Road	
9-10	23.00	100 mm	Biuminous Road	
10-11	26.00	100 mm	Biuminous Road	
11-12	142.00	100 mm	Cement Concrete	
12-13	91.00	100 mm	Cement Concrete	
13-14	25.00	100 mm	Biuminous Road	
14-15	26.00	100 mm	Biuminous Road	
15-16	21.00	100 mm	Biuminous Road	
16-17	25.00	100 mm	Biuminous Road	
17-18	83.00	100 mm	Cement Concrete	
18-19	23.00	100 mm	Biuminous Road	
19-8	23.00	100 mm	Biuminous Road	
15-20	175.00	100 mm	Cement Concrete	
20-21	29.00	100 mm	Biuminous Road	
21-22	22.00	100 mm	Cement Concrete	
22-25	96.00	100 mm	Cement Concrete	
25-26	89.00	100 mm	Cement Concrete	
26-3	23.00	100 mm	Cement Concrete	
20-23	27.60	100 mm	Biuminous Road	
23-24	22.60	100 mm	Biuminous Road	
24-5	116.80	100 mm	Cement Concrete	
2-9	172.20	100 mm	Cement Concrete	
13-27	31.00	100 mm	Biuminous Road	
Total	1532.30			

Table 6.6 Laying of Pipeline on road

6.2.3 Demand Supply of the area

NODE	Nos of	Self demand @ 50 gallon	Peak demand	Self demand
	plots	per capita considering 4	(KL)	in LPS
		storied &20 person in (KL)		
1	0	0.00	0.00	0.00
2	23	104.42	313.26	3.63
3	0	0.00	0.00	0.00
4	0	0.00	0.00	0.00
5	12	54.48	163.44	1.89
6	0	0.00	0.00	0.00
7	15	68.10	204.30	2.36
8	15	68.10	204.30	2.36
9	23	104.42	313.26	3.63
10	0	0.00	0.00	0.00
11	19	86.26	258.78	3.00
12	19	86.26	258.78	3.00
13	20	90.80	272.40	3.15
14	0	0.00	0.00	0.00
15	16	72.64	217.92	2.52
16	0	0.00	0.00	0.00
17	10	45.40	136.20	1.58
18	10	45.40	136.20	1.58
19	0	0.00	0.00	0.00
20	18	81.72	245.16	2.84
21	0	0.00	0.00	0.00
22	13	59.02	177.06	2.05
23	0	0.00	0.00	0.00
24	13	59.02	177.06	2.05
25	26	118.04	354.12	4.10
26	13	59.02	177.06	2.05
Total	265	1203.10	3609.30	41.77

Table 6.7 Demand analysis of the area

Table 6.7 derives the relationship between population size and demand calcucation. Total of 265 are covered under this study, and the node and the plots covered under that plot is tabulated above. Peak factor is taken as 3.0 as per CPHEEO guidelines, also demand has been taken as 50

gallons (190 LPCD) per capita by considering 3 stories and 20 persons per plot. Hence the LPS is Calcuated using per capita demand and multiplying it with the peak factor, that comes out to be 41.77 LPS, that makes the round figure as 42 LPS. Subjected to this per capita demand the reservoir is designed to meet this requirement and deliver 42 LPS of water supply.

6.2.4 Color Coding Of Network

A.Diameter Based

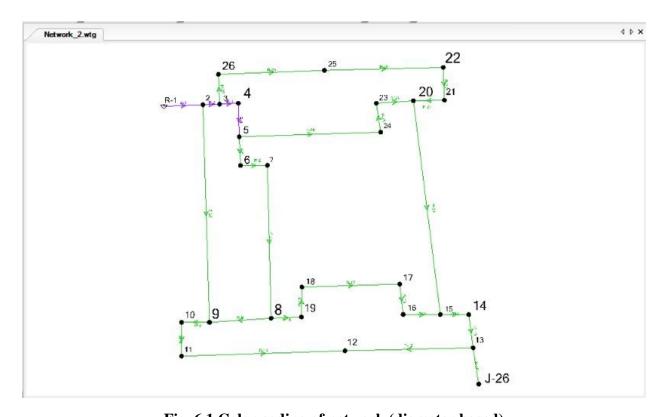


Fig .6.1 Color coding of network (diameter based)

Above Figure(Fig.6.1) shows the color classification of diameter of pipeline of network. This classification simplifies the study and modification of data(if any), if any pipeline is to be changed in the due course of any diameter, this classification will help in modification of that data, for instance If we wish to change the diameter of pipelines P1 and P3, then by directly with the help of color coding we can identify it and modify it according to our requirements. Also it simplifies the study.

Color	Diameter(mm)	Pipelines
Blue	>100	P1,P2,P3,P4
Green	<=100	Others

Table 6.8 Color Coding Classification of diameter

B.Velocity Based

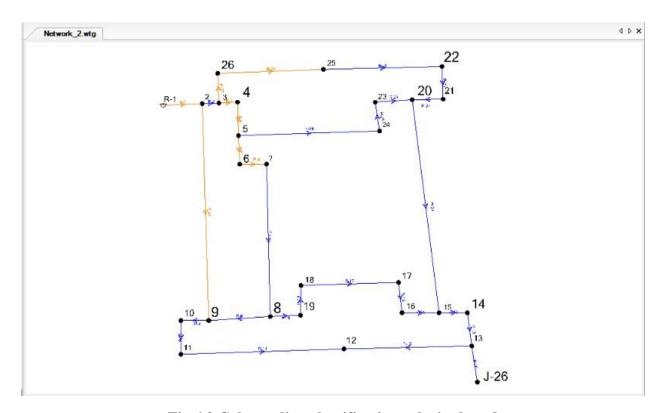


Fig 6.2 Color coding classification velocity based

Above Figure(fig.6.2) shows the color classification of Velocity of flow of pipeline of network. This classification simplifies the study and modification of data, namely(if any), if any pipeline is to be changed in the due course of any parameter, it helps us identify the critical points where flow velocity is above or equal to the maximum flow velocity which might cause cavitation or water hammer phenomena in pipeline, this classification will help in modification of that data, for instance If we wish to determine pipelines with velocity greater than 1.32 m/s, which is the perminted velocity of flow in the water distribution network. Therefore, P1-P5 and P20 and P 28 are the pipelines that carry flow with velocity greater than , then by directly with the help of color

coding we can identify it and provide safety measure, like providing safety valves at these junctions or nodes. Also, it simplifies the study.

Colour code	Velocity(m/s)	Pipelines
orange	>1.25	P1-P5,P 20,P 28
blue	<=1.25	Others

Table 6.9 Color Coding Classification of velocity

C.Head Loss

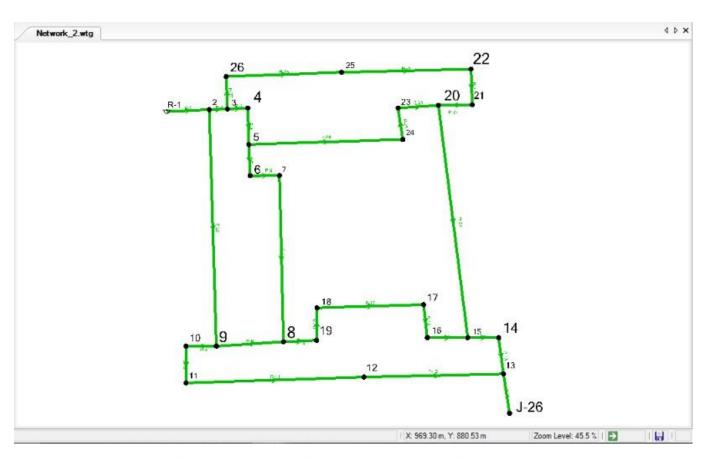


Fig 6.3 Color coding classification on the basis of head loss

Above Figure(fig 6.3) shows the color classification of head loss of pipeline of network. This classification simplifies the study and modification of data(if any), if any pipeline is to be changed in the due course of any Parameter. The CPHEEO recommendations, for the head loss gradient in the water distribution system(WDN), permissible head loss gradient should be equal or less than 1 m/km, so the above figure clearly shows that all 30 pipelines and 26 nodes follows this design crtiteria, as, Head loss is less than designed hence it is satisfied. Also it simplifies the study.

Color	Head Loss Gradient(m/km)
Green	<=1(CPHEEO)

Table 6.10 Color Coding Classification of Head Loss gradient

D.Pressure at Junction(m-H₂O)

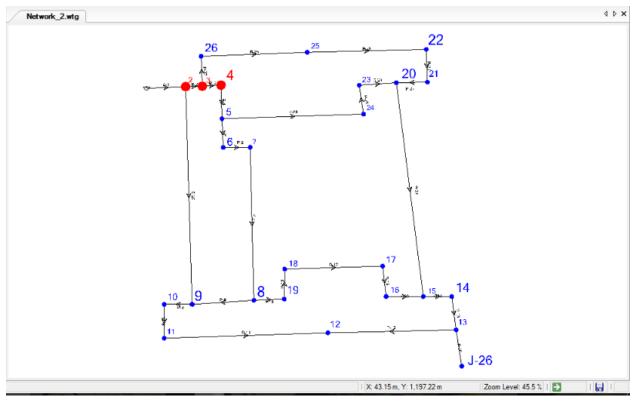


Fig 6.4 Color coding classification on the basis of Pressure at junction

Above Figure(fig 6.4) shows the color classification of pressure at junction of pipeline of network. This classification simplifies the study and modification of data(if any), if any pipeline is to be changed in the due course of any parameter. The CPHEEO recommendations, for the pressure gradient should be less than the total hydraulic head of reservoir, in this case the elevation of reservoir is 22 m, and subsequently as per the design recommendations by CPHEEO, the permissible limit is for one storey7, 17 m for three storied) in the water distribution system(WDN), , so the above figure clearly shows that three pressure junctions(2,3,4) are at risk and hence certain necessary measures have to be adopted to allow them into design criteria. For the present study, residual pressure is taken 17 m for a three storied building.

Color	Residual Pressure(m H ₂ O)
Red	>=17.0
Blue	7.0-17.0

Table 6.11 Color Coding Classification of Pressure at junction

Note: The pressure variation by node and per plot consumption, can be taken into further study, by determining the rate at which pressure is changing or varying when, reservoir is in service. In our study of 265 plots, a total of 26 nodes are covered and 30 pipelines are provided. Number of plots covered by each node is tabulated in following section, and when evey household is taking the maximum supply, the pressure variation at each household can be held into study. But, this study has its shortcomings, as the study will not include the no. of household that have booster or pumps installed at their ends, which will change the pressure and volume of supply considerably.

6.3 MODIFIATIONS OF THE DATA

6.3.1 Modification of diameter

Section 6.1 and 6.2 discussed the validation and results of the network drawn using Bentley WaterGems V8i software, the network was further validated for certain parameters like, head loss gradient, junction pressure ,the pressure which is mandatory for the flow to reach at consumer end.

Further with the study, it was found that few pipelines were not following the design guidelines for the parameters of junction pressure, and by calculations and validation the diameter of pipe has been modified and tabulated as stated below, so the new network will consist this modified values.

Sl.No	Pipe number	Designed Diameter,mm	Modified Diameter,mm
1	P1	150	200
2	P2	150	200
3	P3	150	200
4	P9	150	100
5	P13	150	100
6	P14	150	100
			·
7	P15	150	100

Table 6.12 Modification of diameter of pipelines

6.3.2 Introduction of sluice valves

Sluice valves, (gate valves), are designed to control the flow of fluid through a pipe by raising or lowering a wedge that blocks flow. They are widely used in water and sewer treatment, and come in a wide variety of sizes. Most are designed to open slowly (30-50,360 degree turns of the handle) to prevent opening and closing too rapidly, which causes water hammer.

For the present case study, a total of 9 sluice valves are provided according to the diameter of pipelines, namely 200,150 and 100 mm. Reference to these valves with their pipeline number is tabulated as below:

S.no	Label ID	Pipeline	Diameter of Sluice valve,mm	No.of sluice valve
1	54	P1	200	1
2	56	Р3	150	1
3	60	P7	100	1
4	64	P11	100	1
5	70	P17	100	1
6	73	P20	100	1
7	74	P21	100	1
8	79	P26	100	1
9	82	P28	100	1
TOTAL				9

Table 6.13 Details of Sluice valve

6.3.3 Least cost design

As per the data provided by the Delhi jal Board (DJB),cost of civil works for the laying and jointing of pipes and exacavtion works,laying of thrust blocks,etc is taken as:

Pipe material used	For cast iron(CI)	For ductile iron(DI)
COST OF CIVIL WORK:	Rs. 3,166,622	Rs. 2,910,686

Hence, further total cost of laying and jointing of pipe of material used pipe will be added to the total cost and road restoration charges, removal of surplus malba, labour charges, etc will add up to be the total cost. Hence to obtain the most economical design, both the options had to be be considered. All the rates and estimation cost of civil works and other cost have been inculed with CPWD manual

						(Option I - C.I.)	(Option II - D.I.)
COST OF CIVIL WORK:						Rs. 3,166,622	Rs. 2,910,686
ROAD RESTORATION CHARGES:	Length	Width	Qty	Rate			
Bituminous road up to 12 m	481.20	1.00	481.20	835.52	/sqm	Rs. 402,052	Rs. 402,052
CC Road	1133.00	1.00	1133.00	1064.85	/sqm	Rs. 1,206,475	Rs. 1,206,475
Removal of surplus malba (Bituminous + CC road)	(Sum of	l	1614.20	55.68	/sqm	Rs. 89,879	Rs. 89,879
					Total	Rs. 1,698,406	Rs. 1,698,406
Add 25% enhancement						Rs. 424,601	Rs. 424,601
Total amount of R/R charges						Rs. 2,123,007	Rs. 2,123,007
				TO	TAL:	Rs. 5,289,629	Rs. 5,033,694
ADD 5% FOR CONTIGENCIES:						Rs. 264,481	Rs. 251,685
GRAND TOTAL:						Rs. 5,554,111	Rs. 5,285,378

Table 6.14 Comparison of total cost of pipe materials

Table 6.14 shows the complete abstract of cost, the total cost of civil works is estimated to be ,Rs. 3,166.622 for Option I Cast iron, while For option II i.e. Ductile Iron(DI) pipes ,the total cost is estimated to be Rs. 2,910,686 .All the rates and cost estimation is according to the guidelines of CPWD manual (2014), the revision of rates has been done and the estimation is done on the basis of market rates, so calculation of civil works is obtained by the DJB, and post that, the road restoration charges, addition of 25% enhancements , also adding 5 % for any kind of contingencies,

grand total of the project is calculated that is estimated to be Rs.5,554,111 when cast iron is used as pipe material, while in case of Ductile iron as pipe material it is estimated to be ,Rs 5,285,378.

Therefore, post analysis of least cost design, it is clear, that ductile iron (DI), is the least cost design for the use of pipe material. Also ductile Iron has been accepted widely due to its wide range of benefits.

- DI pipes are recyclable and have this major advantage over Cast iron (CI).
- DI pipes involves little maintenance, hence risk of hazards after installation are lesser as found in cast iron.
- The Flow of supply water increases readily in the DI pipes.
- DI pipes have gained reputation for being at low risk for leakage,.
- Rusting which is a dominant issue for CI pipes, is also eliminated in case for DI pipes, Hence the matter of rusting pipes is also ruled out in these pipes
- DI pipes are considered durable than CI pipes in long run.
- The network in our study has been designed for a span of 30 years so, certainly a durable, effective and efficient material has to be selected .hence Ductile Iron (DI) pipes have been used in our study, which covers a total length of 1615 m of pipeline and 30 pipes in total.

CHAPTER 7

CONCLUSION

7.1 SUMMARY OF THE STUDY

In this thesis, of our present study, design of water distribution network by reliability considerations and least cost analysis performed. Water distribution networks in India were drawn using conventional methods and approximate values of certain parameters was considered and used for the WDN construction, whereas with the evolution of sophisticated computer programmed and softwares, we can build and analyze these type of problems and obtain a better, efficient solution, for a given problem.

Therefore, in our present study,we Understood the the basic principles of creating a Water distribution Network, Furthur with the help of software called BENTLEY WATERGEMS V8i, the network was constructed, of given area of study (B-Block Surajmal Vihar, New Delhi). In the following chapters we validated the network for , satisfaction of the velocity of flow and pressure controls, and Length and diameter with reference to nodal and piplines were tabulated, as per CPHEEO , Nodal demands were satisfied. WDN of surajmal Vihar is designed as per CPHEEO design recommendations, and finally the network is analyzed for least cost, modifications for the network for future studies, were suggested in the final chapter.

However, modelers must take into account, in particular, reliability issues and also monetary limits.

7.2 CONCLUSIONS

The water distribution network of Surajmal vihar (Block-B), New Delhi, has been studied using WATERGEMS software for the following:

- 1. To reduce the head losses at household distributions, pipe size of pipeline connecting the mains and branch line should be increased from half inch to three fourth inch to reduce head losses by 6-7 times.
- 2. A schematic water distribution network is designed as a case study, the design is realized at the basis of the peak hour loading taking peak factor as 3.0 as per CPHEEO guidelines; the necessary modification ,in the diameter are done to provide an efficient system.
- 3. Also the designed reservoir capable of supplying with a flow rate of 42 LPS, seems to be satisfying the demand requirements of the population of over 5000 in the study area.
- 4. The installed capacity of reservoir is 1.2 million litres (1200m³), which is sufficient to meet the demand of population (including the peak factor hourly demand) for next three decades, if required another tank of required capacity could be installed ,or valve operated pipelines can be taken into considerations to increase the flow rates with increase in demand ,after two and half decades, that too if the existing reservoir is not meeting the requirements.
- 5. Total Length of pipeline laid is 1614.20 m,out of which 1133.0 m was laid on Cement concrete road (CC road),and 481.20 m was laid on bituminous road.
- 6. Pipelines P1,P2 have 200 mm diameter pipes, P3,P4 have 150 mm diameter pipeline while other pipleines consists of 100 mm diameter DI pipes.
- 7. Velocity of flow ,as per CPHEEO guidelines, should be in the range of 0.06 m/s to 1.42 m/s,minimum velocity should be maintained to avoid any corrosion and sedimentation in the pipelines, and maximum velocity should not be exceeded to avoid any damage in pipeline due to water hammer,phenomenan .Hence in our study all 26 nodes and 30 pipelines follows these design criteria and maximum velocity in the network is 1.32 m/s,and some pipelines have zero velocity,because of no demand during average daily demand,while some velocity is achived at the time of peak flow.

- 8. Head loss gradient, as per design criteria should be less than 1 m/km for water supply network. In our study, the head loss gradient is computed directly using hazen William equation by WaterGems software, and the values comes to be satisfaying the design criteria, head loss gradient for the water supply network is in the range 0.000 -0.0035 m/m. Hence, the network is within safe design criteria.
- 9. Pressure at junctions,i.e.Nodal Pressure as per design criteria should be within permissible limits, which is defined by CPHEEO between 7 m to 17 m for this distribution system. Also,if every household is taking the maximum supply,the pressure variation at each household can be held into study. But, this study has its shortcomings, as the study will not include the no.of household that have booster or pumps installed at their ends,which will change the pressure and volume of supply at other households considerably.
- 10. In our case study,three junctions were at risk of violating this design criteria namely, Nodes 2,3 and 4, which was analysed from the watergems color coding criteria of pressue junctions. Hence to safeguard these nodes or junctions, diameters of the pipelines assocated with these nodes were modified . So, pipeline P1, P2 and P3 were modified to 200 mm, while to counterbalance the economy of overall network, P13, P14, and P15 pipelines diameters changed to 100 mm respectively.
- 11. Sluice valves are introduced, these valves are used to control the flow, these valves are used for the control and frequent operation. For our study of WDN,comprises of 9 sluice valves of diameters 200,150 and 100 mm are installed respectively one sluice value installed at pipeline P1,P3 respectively of 200 and 150 mm diameters respectively ,while six valves of 100 mm diameters are installed at pipelines P7,P11,P17,P20,P21,P26,P28.
- 12. And Finally as per least cost design analysis of the network, that includes civil works, road restoration charges, removal of surplus waste, addition of 25% enhancements and 5% for any kind of contingencies. The economical design for this system is the use of Ductile Iron (DI) material for pipelines.

The network constructed with the help of Watergems, is therefore successfully validated for various design parameters.

7.3 SCOPE FOR FUTURE WORK

The future work for this study will mainly deal with the improvements of the Linear Programming algroithims, which is coded in this study. The most important step for the future work is to include node isolation approach for the decision making process for improving the network, if a limited amount of money is available. This study, could be further carried for the detection of accidental contamination in a water distribution network, conceptually, the study could be carried out in the network to detect internal deterioration of water quality in a distribution network. Also, valve operated pipelines that are installed could be utilized to satisfy the nodal demands in future.

Also, Another important step for the Software WaterGems will be convention of pumps and tank element, for instance, with the growing population of the area, there might arise a need of installation of new tanks or reservoirs, whose study could be simplified with the help of use of WaterGems V8i in the network. Also, the optimization model should be coupled with simuation techniques to determine tank diameters, elevations, and locations that meet the required Preflow durations and storage volumes, Furthur it may be aimed to better model pressure-sensitive nodal pressures during a pre event and obtain a more accurate estimate of ex-pected conditional Pre damages.

Determination of Chlorine residuals in water distribution systems in another important future study, use of single decay constant for all pipes in a network may not seem suitable for certain distribution systems. For future researches and study, primary objective could be to apprehend how this decay constant might be determined by pipe characteristics, such as network age or pipe material, also flow supply characteristics indicative of bio film occurrence or any form of corrosion activity. The chlorine decay model and its implementation within the softwares like EPANET or Water Gems program will deliver water-supply engineers and designers with a valuable tool for understanding the performance of chlorine residuals through their system, under a wide range of variety according to varying hydraulic conditions. A more user friendly interface is aimed for the future versions of the program.

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