CHAPTER-5

CASE STUDIES AND RESULTS:

To test the convergence of the developed model, a number of case studies were carried out on a simple 6-bus system and the 30-bus system. In each of these test systems a TCSC is incorporated. In all these case studies, a convergence tolerance of 10⁻⁴ has been chosen. The case studies are elaborated below:

Case 1: This is a base case without a TCSC for the 6-Bus system. The 6-Bus system (Line & Bus Data is attached in Appendix) used for implementing TCSC is shown in Fig 5.1 below. A power flow solution yielded results tabulated in 5.1 and voltage versus bus no plot is shown in Fig 5.2

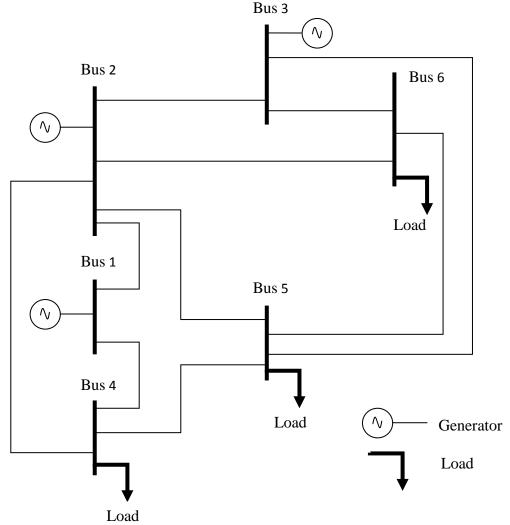


Fig 5.1 6-Bus system used for Implementing TCSC

Table 5.1 Basecase powerflow solution of 6-Bus system

| Bus No. | Voltage | Phase angle |
|---------|---------|-------------|
| Dus No. | (p.u.) | (Degrees) |
| 1 | 1.0500 | 0 |
| 2 | 1.0500 | -3.6712 |
| 3 | 1.0700 | -4.2733 |
| 4 | 0.9894 | -4.1958 |
| 5 | 0.9854 | -5.2764 |
| 6 | 1.0044 | -5.9475 |

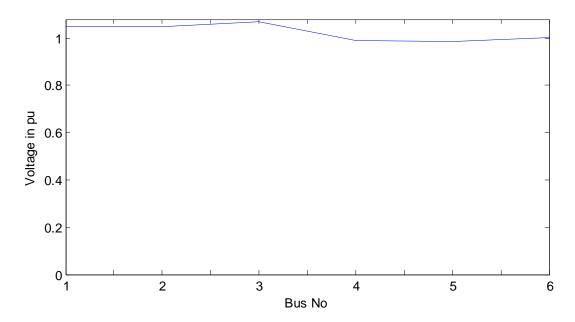


Fig .5.2 Voltage profile for 6-Bus system

Case 2: This is a case with TCSC installed between line 2 and Line 5 and power flow in the line increased from 0.1502 p.u to 0.2 p.u. A power flow solution yielded results tabulated in 5.2 and voltage versus bus no plot is shown in Fig 5.3

Table 5.2 Powerflow solution of 6-Bus system with TCSC

| Bus No. | Voltage | Phase angle | Susceptance | Firing Angle | | |
|------------------------------|---------|-------------|----------------------------------|-------------------|--|--|
| Dus No. | (p.u.) | (Degrees) | (p.u.) | (Degrees) | | |
| 1 | 1.0500 | 0 | | | | |
| 2 | 1.0500 | -4.3386 | | | | |
| 3 | 1.0700 | -4.8825 | $B_{TCSC} = 1.8913 \text{ p.u.}$ | $\alpha = 167.54$ | | |
| 4 | 0.9810 | -4.4946 | $\alpha = 166.57$ | | | |
| 5 | 0.9274 | -4.3865 | | | | |
| 6 | 0.9932 | -6.3944 | | | | |
| $P_{2-5} = 0.2 \text{ p.u.}$ | | | | | | |

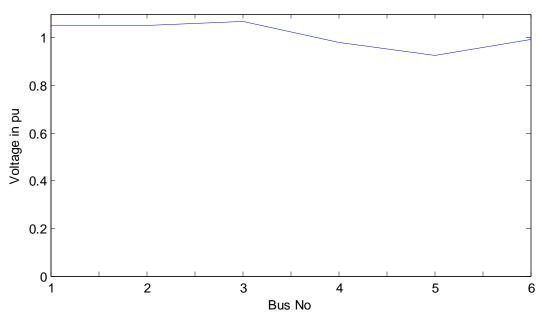


Fig .5.3 Voltage profile for the 6-Bus system with TCSC in line 2-5

The complete Powerflow solution for the 6-Bus system after implementing TCSC is tabulated in Table 5.5. TCSC is placed in Line between 2&5, the percentage increase in Line is 33.15% and the number of iterations is 17 in case of Alfa model and 7 in case of Susceptance model. The Btcsc value in both the cases should be the same which is 1.8913 p.u.

Case 3: This is a case with TCSC installed between line 3 and Line 5 and power flow in the line increased from 0.1802 p.u to 0.25 p.u. A power flow solution yielded results tabulated in 5.3 and voltage versus bus no plot is shown in Fig 5.4

Table 5.3 Powerflow solution of 6-Bus system with TCSC

| Bus No. | Voltage | Phase angle | Susceptance | Firing Angle | | |
|-------------------------------|---------|-------------|----------------------------------|-------------------|--|--|
| | (p.u.) | (Degrees) | (p.u.) | (Degrees) | | |
| 1 | 1.0500 | 0 | | | | |
| 2 | 1.0500 | -4.2914 | | | | |
| 3 | 1.0700 | -5.4547 | $B_{TCSC} = 1.8376 \text{ p.u.}$ | $\alpha = 172.06$ | | |
| 4 | 0.9799 | -4.4687 | $\alpha = 171.78$ | | | |
| 5 | 0.9207 | -4.7138 | | | | |
| 6 | 0.9915 | -6.7138 | | | | |
| $P_{3-5} = 0.25 \text{ p.u.}$ | | | | | | |

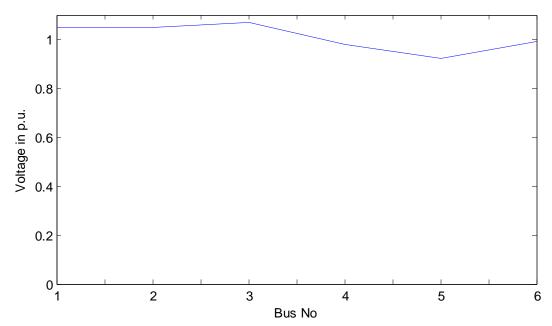


Fig .5.4 Voltage profile for the 6-Bus system with TCSC in line 3-5

The complete Powerflow solution for the 6-Bus system after implementing TCSC is tabulated in Table 5.5. TCSC is placed in Line between 3&5, the percentage increase in Line is 38.73% and the number of iterations is 19 in case of Alfa model and 12 in case of Susceptance model. The Btcsc value in both the cases should be the same which is 1.8376 p.u.

Table 5.5 Complete Powerflow solution obtained in case of 6- bus system

| From | То | Base | Power | Percent | Power Flow Solution | | | | | | | |
|------|--------------|---------------|--------------|-----------------|-----------------------|------------------------|------------|-----------------------|-----------------------|------------------------|------------|-----------------------|
| Bus. | Bus. no | case Power | flow with | change in Power | | Alpha Model | | | Susceptance Model | | | |
| | | flow (pu) | TCSC (pu) | flow (%) | No. of iterations 't' | Time taken (sec) | Btcsc (pu) | Firing angle (degree) | No. of iterations 't' | Time taken (sec) | Btcsc (pu) | Firing angle (degree) |
| | 6-Bus system | | | | | | | | | | | |
| 2 | 5 | 0.1502 | 0.2000 | 33.15 | 17 | 0.1453 | 1.8913 | 167.54 | 7 | 0.1513 | 1.8913 | 166.57 |
| | | | | | | | | | | | | |
| 3 | 5 | 0.1802 | 0.2500 | 38.73 | 19 | 0.1390 | 1.8376 | 172.06 | 12 | 0.1529 | 1.8376 | 171.78 |
| | | | | | | | | | | | | |

Case 4: This is a base case without a TCSC for the 30-Bus system. The 30-Bus system (Line & Bus Data is attached in Appendix) used for implementing TCSC is shown in Fig 5.5. A power flow solution yielded results tabulated in 5.6 and voltage versus bus no plot is shown in Fig 5.6

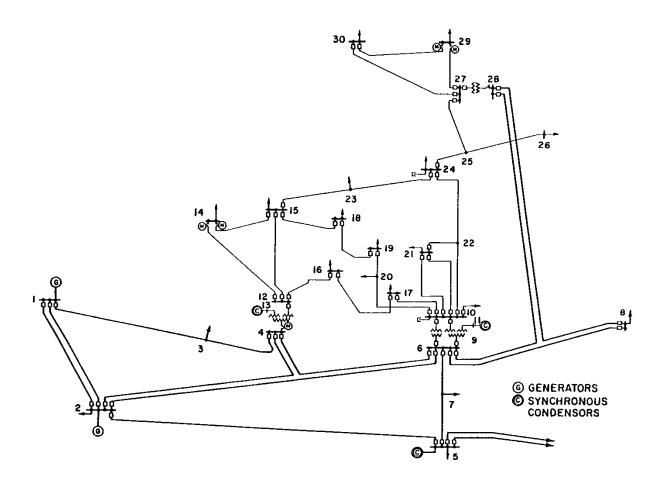


Fig 5.5 IEEE 30-Bus test system

Table 5.6 Basecase powerflow solution of 30-Bus system

| Bus No. | Voltage | Phase angle | Bus No. | Voltage | Phase angle |
|---------|---------|-------------|---------|---------|-------------|
| | (p.u.) | (Degrees) | Dus No. | (p.u.) | (Degrees) |
| 1 | 1.0600 | 0 | 16 | 1.0425 | -16.0433 |
| 2 | 1.0430 | -5.3539 | 17 | 1.0379 | -16.2894 |
| 3 | 1.0100 | -14.1813 | 18 | 1.0261 | -17.0422 |
| 4 | 1.0100 | -11.8393 | 19 | 1.0236 | -17.1807 |
| 5 | 1.0820 | -14.4177 | 20 | 1.0277 | -16.9644 |

| Bus No. | Voltage | Phase angle | Bus No. | Voltage | Phase angle |
|---------|---------|-------------|---------|---------|-------------|
| Dus No. | (p.u.) | (Degrees) | Dus No. | (p.u.) | (Degrees) |
| 6 | 1.0710 | -15.5556 | 21 | 1.0307 | -16.5359 |
| 7 | 1.0208 | -7.5240 | 22 | 1.0312 | -16.5233 |
| 8 | 1.0119 | -9.2741 | 23 | 1.0250 | -16.8178 |
| 9 | 1.0100 | -11.0848 | 24 | 1.0193 | -16.9140 |
| 10 | 1.0022 | -12.8835 | 25 | 1.0154 | -16.4418 |
| 11 | 1.0500 | -14.4177 | 26 | 0.9977 | -16.8631 |
| 12 | 1.0431 | -16.0860 | 27 | 1.0216 | -15.8888 |
| 13 | 1.0550 | -15.5556 | 28 | 1.0065 | -11.7151 |
| 14 | 1.0401 | -16.4229 | 29 | 1.0017 | -17.1229 |
| 15 | 1.0356 | -16.4855 | 30 | 0.9902 | -18.0088 |

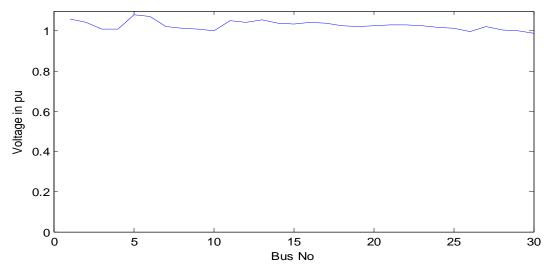


Fig .5.6 Voltage profile for 30-Bus system (base case)

Case 5: This is a case with TCSC installed between line 14 and Line 15 and power flow in the line increased from 0.0142 to 0.016 p.u. A power flow solution yielded results tabulated in 5.7 and voltage versus bus no plot is shown in Fig 5.7

Table 5.7 Powerflow solution of 6-Bus system with TCSC (Line 14-15)

| Bus No. | Voltage | Phase angle | Bus No. | Voltage | Phase angle | | |
|---------|---|-----------------|------------|---------|-------------|--|--|
| Bus No. | (p.u.) | (Degrees) | Dus No. | (p.u.) | (Degrees) | | |
| 1 | 1.0600 | 0 | 16 | 1.0222 | -15.9474 | | |
| 2 | 1.0430 | -5.3397 | 17 | 1.0184 | -16.2475 | | |
| 3 | 1.0100 | -14.1358 | 18 | 1.0039 | -16.9451 | | |
| 4 | 1.0100 | -11.7874 | 19 | 1.0022 | -17.1256 | | |
| 5 | 1.0820 | -14.3547 | 20 | 1.0069 | -16.9192 | | |
| 6 | 1.0710 | -15.3828 | 21 | 1.0109 | -16.5174 | | |
| 7 | 1.0268 | -7.60770 | 22 | 1.0112 | -16.5015 | | |
| 8 | 1.0193 | -9.37090 | 23 | 1.0019 | -16.6949 | | |
| 9 | 1.0137 | -11.0983 | 24 | 0.9970 | -16.8551 | | |
| 10 | 1.0044 | -12.8712 | 25 | 0.9902 | -16.3539 | | |
| 11 | 1.0357 | -14.3547 | 26 | 0.9720 | -16.7973 | | |
| 12 | 1.0241 | -16.0587 | 27 | 0.9948 | -15.7714 | | |
| 13 | 1.0341 | -15.3828 | 28 | 1.0098 | -11.7088 | | |
| 14 | 1.0257 | -16.4957 | 29 | 0.9743 | -17.0742 | | |
| 15 | 1.0121 | -16.3029 | 30 | 0.9625 | -18.0112 | | |
| | | $P_{14-15} = 0$ | 0.016 p.u. | • | • | | |
| | $B_{TCSC} = 1.4235 \text{ p.u.}; \ \alpha = 169.65$ | | | | | | |
| | α=171.35 | | | | | | |

The complete Powerflow solution for the 30-Bus system after implementing TCSC is tabulated in Table 5.9. TCSC is placed in Line between 14&15, the percentage increase in Line is 12.67% and the number of iterations is 10 in case of Alfa model and 7 in case of Susceptance model. The Btcsc value in both the cases should be the same which is 1.4235 pu.

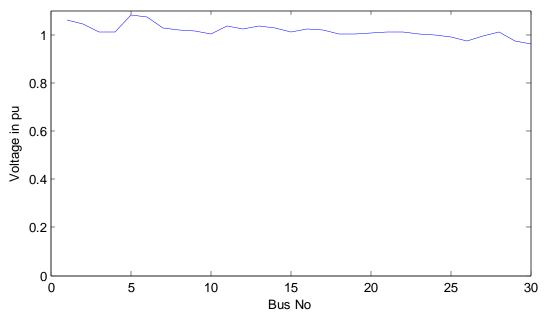


Fig .5.7 Voltage profile for the 30-Bus system with TCSC in line 14-15

Case 6: This is a case with TCSC installed between line 13 and Line 15 and power flow in the line increased from 0.169 p.u. to 0.190 p.u . A power flow solution yielded results tabulated in 5.8 and voltage versus bus no plot is shown in Fig 5.8

Table 5.8 Powerflow solution of 6-Bus system with TCSC (Line 13-15)

| Bus No. | Voltage (p.u.) | Phase angle (Degrees) | Bus No. | Voltage (p.u.) | Phase angle (Degrees) |
|---------|----------------|-----------------------|---------|----------------|-----------------------|
| 1 | 1.0600 | 0 | 16 | 1.0224 | -16.3037 |
| 2 | 1.0430 | -5.3960 | 17 | 1.0068 | -16.3876 |
| 3 | 1.0100 | -14.2199 | 18 | 0.9490 | -15.5412 |
| 4 | 1.0100 | -11.8897 | 19 | 0.9591 | -16.2393 |
| 5 | 1.0820 | -14.3680 | 20 | 0.9702 | -16.2743 |
| 6 | 1.0710 | -15.1018 | 21 | 0.9912 | -16.4453 |
| 7 | 1.0267 | -7.7330 | 22 | 0.9906 | -16.3976 |
| 8 | 1.0192 | -9.5267 | 23 | 0.9455 | -15.1395 |
| 9 | 1.0123 | -11.1785 | 24 | 0.9652 | -16.2676 |
| 10 | 1.0036 | -12.9536 | 25 | 0.9682 | -16.1734 |
| 11 | 1.0272 | -14.3680 | 26 | 0.9496 | -16.6376 |

| Bus No. | Voltage | age Phase angle Bus I | | Voltage | Phase angle | | |
|---|---------------------------------|-----------------------|---------|---------|-------------|--|--|
| Dus No. | (p.u.) | (Degrees) | Dus No. | (p.u.) | (Degrees) | | |
| 12 | 1.0074 | -16.0624 | 27 | 0.9793 | -15.8207 | | |
| 13 | 1.0464 | -16.1016 | 28 | 1.0072 | -11.7616 | | |
| 14 | 0.9823 | -16.0786 | 29 | 0.9584 | -17.1662 | | |
| 15 | 0.9380 | -13.9504 | 30 | 0.9464 | -18.1349 | | |
| | $P_{13-15} = 0.19 \text{ p.u.}$ | | | | | | |
| $B_{TCSC} = 2.3374 \text{ p.u.}; \ \alpha = 171.52$ | | | | | | | |
| $\alpha = 171.37$ | | | | | | | |

The complete Powerflow solution for the 30-Bus system after implementing TCSC is tabulated in Table 5.9. TCSC is placed in Line between 13&15, the percentage increase in Line is 12.43% and the number of iterations is 39 in case of Alfa model and 11 in case of Susceptance model. The Btcsc value in both the cases should be the same which is 2.3374 p.u.

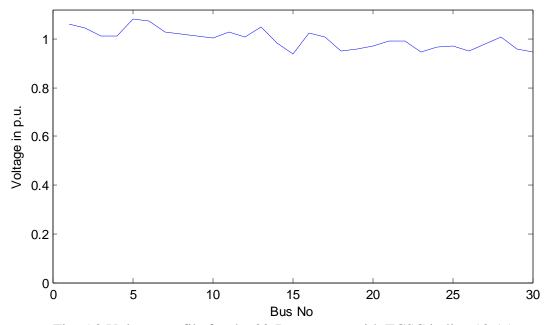


Fig .5.8 Voltage profile for the 30-Bus system with TCSC in line 13-15

Table 5.9 Complete Powerflow solution obtained in case of 30- bus system

| From | То | Base | Power | Percent | Power Flow Solution | | | | | | | |
|------------|---------------|---------------|--------------|-----------------|-----------------------|------------------------|------------|-----------------------|-----------------------|------------------------|------------|-----------------------|
| Bus. no | Bus. | case Power | flow with | change in Power | Alpha Model | | | Susceptance Model | | | | |
| | | flow (pu) | TCSC (pu) | flow (%) | No. of iterations 't' | Time taken (sec) | Btcsc (pu) | Firing angle (degree) | No. of iterations 't' | Time taken (sec) | Btcsc (pu) | Firing angle (degree) |
| | 30-Bus system | | | | | | | | | | | |
| 14 | 15 | 0.0142 | 0.0160 | 12.67 | 10 | 0.162 | 1.4235 | 171.35 | 7 | 0.140 | 1.4235 | 169.65 |
| | • | | | | | | | | | | | |
| 13 | 15 | 0.1690 | 0.1900 | 12.43 | 39 | 0.256 | 2.3374 | 171.37 | 11 | 0.185 | 2.3374 | 171.52 |
| | • | | • | | | | | • | | • | • | |

CHAPTER-6

CONCLUSION:

In this work, a Newton power flow model of the Thyristor Controlled Series Capacitor (TCSC) was developed. The model was appropriately modified to include both the susceptance and the firing angle model of the TCSC. Power flow case studies were carried out with TCSCs installed in different lines in a small six bus system and the IEEE 30 bus system. Power flow solutions were obtained for both the susceptance and the firing angle models. Solution values displayed a close match for both the models. In all the case studies, very good convergence characteristics were obtained, which validates the model

FUTURE SCOPE OF WORK:

Multiple TCSCs can be incorporated into the system by making some changes in the jacobian matrix of the system. An additional row and column are added in the jacobian matrix to incorporate an extra TCSC installed in the system. The susceptance model and firing angle model will have the same number of iterative loops but yield individual alpha values of the TCSCs.

The project can also be developed by using Fast decoupled load flow instead of Newton-Raphson powerflow for fast convergence and computational time.

REFERENCES

- [1]N.G.Hingorani and L.Gyugyi, "Understanding FACTS, Concepts and Technology of Flexible AC Transmission Systems", IEEE Press, 2000.
- [2]R.M.Mathur and R.K.Varma, "Thyristor-based FACTS Controllers for Electrical Transmission Systems", 1st Edition, Wiley-Interscience, New York, 2002.
- [3] A. J. Wood, B.F. Wollenberg, "Power Generation, Operation, and Control", 2nd Edition, John Wiley and Sons, New York, 1996.
- [4] Enrique Acha, Vassilios Agelidis, Olimpo Anaya, TJE Miller.," Power Electronic Control in Electrical Systems", 1st Edition, Newnes Power Engineering Series, 2002.
- [5] N.G.Hingorani, "Power Electronics in Electrical utilities: Role of Power Electronics in Future Power Systems", Proceedings of the IEEE Vol. 76 No. 4, April 1988, pp. 481-482
- [6] N. G.Hingorani, "Flexible AC transmission systems", IEEE Spectrum, April. 1993, pp. 4045.
- [7] N.G.Hingorani," FACTS technology and opportunities", IEE Colloquium on Flexible AC Transmission Systems (FACTS) The Key to Increased Utilization of Power Systems, (Digest No.1994/005), Jan 1994,pp. 4/1-410.
- [8] N.G.Hingorani, "FACTS Technology State of the Art, Current Challenges and the Future Prospects", Power Engineering Society General Meeting, IEEE, 2007, pp. 1-4.
- [9] Naresh Acharya, Arthit Sode-Yome, Nadarajah Mithulananthan, "Facts about Flexible AC Transmission Systems (FACTS) Controllers: Practical Installations and Benefits", Australian Universities Power Engineering Conference (AUPEC) ,September 2005, Vol.2, pp.184-189

- [10]C. Gama, Angquist, G. Ingeström, M. Noroozian, "Commissioning and operative experience of TCSC for damping power oscillation in the Brazilian North-South interconnection", CIGRE, Session 2000.
- [11] Ghamandi Lal, Dipak Dutta, M.Arunachalam, "Design and Testing of Thyristor valves of TCSC for Kanpur-Ballabhgarh 400kV line", IEEE/PES, Transmission and Distribution Conference and Exposition, 2008, pp. 1-6.
- [12] Xiaoxin Zhou, Jianbo Guo, Qiang Guo, "Studies on Application of TCSC in power systems of China", IEEE EPSR (2000),pp. 387-390.
- [13] S. Meikandasivam, Rajesh Kumar Nema, and Shailendra Kumar Jain, "Performance of Installed TCSC Projects", India International Conference on Power Electronics (IICPE), 2010.
- [14] ABB, North South 500 kV AC power interconnection: transmission stability improvement by means of TCSC at Eletronorte of Brazil and SC, ABB power technologies ABB, www.abb.com/powersystems.
- [15] R. Grunbaum, Jacques Pernot, ABB, "Thyristor-controlled series compensation: A state of the art approach for optimization of transmission over power links", www.abb.com.
- [16] ABB, "TCSC for stable transmission of surplus power from eastern to western India", ABB power technologies, www.abb.com/powersystems.
- [17] E. Larsen, C.Bowler, B. Damsky, S. Nillson, "Benefits of TCSC", Cigre Paper 14/37, Paris 1992,pp. 38-04.
- [18] Xiang Zheng, Zheng Xu, and Jing Zhang, "A Supplementary Damping Controller of TCSC for Mitigating SSR", IEEE Power & Energy Society General Meeting, July 2009,pp.1-5.

- [19] MD. Nasimul islam maruf, A.S.M. Moshin and MD. Asaduzzaman shoeb, "Study of Thyristor controlled series capacitor (TCSC) as a useful device", International Journal of Engineering Science and Technology, Vol. 2(9), 2010, pp. 4357-4360.
- [20]Antonio.C.Borre, AbneryOrtiz, H.Edson Watanabe and Waldemar Sulkowski, "Synchronous Generator Power Oscillations Damped by Using TCSC or SSSC Working as a Variable Reactance", Electrical Machines and Systems (ICEMS), August, 2011, pp. 1-6.
- [21]Zhao Xueqiang and Chen Chen, "Circuit Analysis of a Thyristor Controlled Series Compensation", IEEE Power Engineering Society Winter Meeting, February 1999, Vol No.2,pp . 1067 1072.
- [22] A.K.Sahoo, S.S.Dash and T.Thyagarajan, "Power Flow Study Including FACTS Devices", Journal of Applied Sciences, 2010, pp. 1563-1571.
- [23] Douglas J. Gotham, G. T. Heydt," Power Flow Control and Power Flow Studies for systems with FACTS Devices", IEEE Transactions on Power Systems, Vol. 13, No. 1, February 1998,pp. 60-65.
- [24] William F.Tinney, "Power Flow Solution by Newton's Method", IEEE Transactions on Power Apparatus and Systems, Vol. PAS-86, No.11, November 1967, pp. 1449-1967.
- [25] C. R. Fuerte-Esquivel, E. Acha, and H. Ambriz-PBrez, "A Thyristor Controlled Series Compensator Model for the Power Flow Solution of Practical Power Networks", IEEE Transactions on power systems, Feb 2000, Vol. 15 (1), pp. 58-64.
- [26] Dragan Jovcic, and G. N. Pillai, "Analytical Modeling of TCSC Dynamics," IEEE Transactions on Power Delivery, Vol. 20, No. 2, April 2005,pp. 1097 1104.
- [27] Ambriz-Pérez H, C.R.Fuerte-Esquivel, E. Acha, "TCSC-firing angle model for optimal power flow solutions using Newton's method", International Journal of Electrical Power & Energy Systems, Vol. 28, No. 2, February 2006, Pages 77-85.

- [28] M.A.Abdel Moamen and N.P.Padhy, "Newton-Raphson TCSC Model for Power Flow Solutions of Practical Power Networks", Proceedings of IEEE Summer Meeting vol.3, July 2002, pp. 1488 1493.
- [29] Guowen H U, Ming CHENG and Guilong CAI, "Relation between Fundamental Frequency Equivalent Impedance and Resonant Point for Thyristor Controlled Series Compensation", Annual Conference of the IEEE Industrial Electronics Society, November 2004.
- [30] Power System Test Archive UWEE (University of Washington). [Online] http://www.ee.washington.edu/research/pstca
- [31] N.G.Hingorani, "FACTS Flexible AC Transmission systems", Electric Power Research Institute (EPRI), USA.
- [32] Philip Moore, P.Ashmole, "Flexible AC Transmission systems", Power engineering journal IEEE, Dec 1995, Vol.9(6), pp.282-286.
- [33] Peter Fairly, "Flexible AC Transmission: The FACTS Machine", IEEE Spectrum, January 2011.
- [34] IEEE Power Engineering Society/ CIGRE," FACTS Overview", Publication 95TP108, IEEE Press, New York, 1995.
- [35] L. Gyugyi, K. K. Sen and C. D. Schauder, "The interline power flow controller concept a new approach to power flow management in transmission systems", IEEE Transactions on Power Delivery Vol. 14(3), pp.1115-1123.
- [36] Federico Milan, "Continuous Newton's Method for Power Flow Analysis", IEEE Transactions on Power Systems, Vol. 24, No. 1, Feb 2009,pp. 50-57.

- [37] C. R. Puerle-Esquivel and E. Acha, "A Newton-type algorithm for the control of power flow in electrical power networks", IEEE Transactions on Power Systems, Vol. 12,No. 4,November 1997, pp. 1474-1480.
- [38] C.R Fuerte Esquivel, E.Acha, "Newton-Raphson algorithms for the reliable solution of large power networks with embedded FACTS devices", IEE proceedings on generation, transmission, distribution, Vol 143, No.5, September 1996,pp. 447 454.
- [39] Bindeshwar Singh, N. K. Sharma and A. N. Tiwari, and S.P.Singh, "Incorporation of FACTS Controllers in Newton Raphson Load Flow for Power Flow Operation, Control and Planning: A Comprehensive Survey", International Journal on Computer Science and Engineering, (IJCSE), Vol.02, No. 06, 2010.
- [40]A.Ghosh and G.Ledwich, "Modeling and control of thyristor controlled series compensators", Proceedings in IEE Generation, Transmission, Distribution, vol. 142, May 1995, pp. 297–304.
- [41] Scott J.G.Mey, William A.Mittelstadt, Randy.W.Suhrbier, "Test Results and Initial Operating Experience for the BPA 500 kV Thyristor Controlled Series Capacitor Design, Operation, and Fault Test Results", Northcon conference, October 1995,pp.265-273.
- [42]N Christl,R Hedig, K.Sadek, P.Lutzelberger, P.E.Krause, S.M.McKenna, A.H.Montonyo, and D.togerson, "Advanced Series Compensation (ASC) with Thyristor-Controlled Impedance," paper 14/37/38-05, CIGRE, Paris, 1992.
- [43] N Christl, R Hedig R Johnson, P Krause, and A Montoya," Power System Studies and Modeling for the Kayenta 230 kV Substation Advanced Series Compensation", International Conference on AC and DC Power Transmission,1991, pp. 33-37.
- [44] Muhammad H. Rashid, "Power Electronics (concept of Flexible AC Transmission Systems)", Pearson Education-3rd Edition, 2004.

APPENDIX

Table 6.1 Line Data for the 6-Bus system [3]

| From bus | To bus | R(pu) | X(pu) | BCAP*(pu) |
|----------|--------|-------|-------|-----------|
| 1 | 2 | 0.10 | 0.20 | 0.020 |
| 1 | 4 | 0.05 | 0.20 | 0.020 |
| 1 | 5 | 0.08 | 0.30 | 0.030 |
| 2 | 3 | 0.05 | 0.25 | 0.030 |
| 2 | 4 | 0.05 | 0.10 | 0.010 |
| 2 | 5 | 0.10 | 0.30 | 0.020 |
| 2 | 6 | 0.07 | 0.20 | 0.025 |
| 3 | 5 | 0.12 | 0.26 | 0.025 |
| 3 | 6 | 0.02 | 0.10 | 0.010 |
| 4 | 5 | 0.20 | 0.40 | 0.040 |
| 5 | 6 | 0.10 | 0.30 | 0.030 |

BCAP *= half total line charging susceptance

Table 6.2 Bus data for the 6-Bus system

| Bus number | Bus type | Voltage schedule(pu V) | P _{gen} (pu MW) | P _{load} (pu MW) | Q _{load} (pu MVAR) |
|------------|-----------|------------------------------|--------------------------|---------------------------|-----------------------------|
| 1 | Swing | 1.05 | | | |
| 2 | Generator | 1.05 | 0.5 | 0.0 | 0.0 |
| 3 | Generator | 1.07 | 0.6 | 0.0 | 0.0 |
| 4 | Load | | 0.0 | 0.7 | 0.7 |
| 5 | Load | | 0.0 | 0.7 | 0.7 |
| 6 | Load | | 0.0 | 0.7 | 0.7 |

The above Table 6.1 &6.2 list the input data for the six-bus system used in the Project [3]. The impedances are per unit on a base of 100 MVA.

Table 6.3 Line Data for 30-Bus system [30]

| From bus | To bus | R(pu) | X(pu) | BCAP* (pu) | From bus | To bus | R(pu) | X(pu) | BCAP* (pu) |
|----------|--------|--------|--------|------------|----------|--------|----------|--------|------------|
| 1 | 2 | 0.0192 | 0.0575 | 0.0264 | 15 | 18 | 0.1073 | 0.2185 | 0 |
| 1 | 7 | 0.0452 | 0.1652 | 0.0204 | 18 | 19 | 0.0639 | 0.1292 | 0 |
| 2 | 8 | 0.0570 | 0.1737 | 0.0184 | 19 | 20 | 0.0340 | 0.0680 | 0 |
| 7 | 8 | 0.0132 | 0.0379 | 0.0042 | 12 | 20 | 0.9360 | 0.2090 | 0 |
| 2 | 3 | 0.0472 | 0.1983 | 0.0209 | 12 | 17 | 0.0324 | 0.0845 | 0 |
| 2 | 9 | 0.0581 | 0.1763 | 0.0187 | 12 | 21 | 0.0348 | 0.0749 | 0 |
| 8 | 9 | 0.0199 | 0.0414 | 0.0045 | 12 | 22 | 0.0727 | 0.1499 | 0 |
| 3 | 10 | 0.0460 | 0.1160 | 0.0102 | 21 | 22 | 0.0116 | 0.0236 | 0 |
| 9 | 10 | 0.0267 | 0.082 | 0.0085 | 15 | 23 | 0.1000 | 0.2020 | 0 |
| 9 | 4 | 0.0120 | 0.0420 | 0.0045 | 22 | 24 | 0.1150 | 0.1790 | 0 |
| 9 | 11 | 0 | 0.2080 | 0 | 23 | 24 | 0.1320 | 0.2700 | 0 |
| 9 | 12 | 0 | 0.5560 | 0 | 24 | 25 | 0.1885 | 0.3292 | 0 |
| 11 | 5 | 0 | 0.2080 | 0 | 25 | 26 | 0.2544 | 0.3800 | 0 |
| 11 | 12 | 0 | 0.1100 | 0 | 25 | 27 | 0.1093 | 0.2087 | 0 |
| 8 | 13 | 0 | 0.2560 | 0 | 28 | 27 | 0.3960 | 0.3960 | 0 |
| 13 | 6 | 0 | 0.1400 | 0 | 27 | 29 | 0.2198 | 0.4153 | 0 |
| 13 | 14 | 0.1231 | 0.2599 | 0 | 27 | 30 | 0.3202 | 0.6027 | 0 |
| 13 | 15 | 0.0662 | 0.1304 | 0 | 29 | 30 | 0.2399 | 0.4533 | 0 |
| 13 | 16 | 0.0945 | 0.1987 | 0 | 4 | 28 | 0.0636 | 0.2000 | 0.0214 |
| 14 | 15 | 0.2210 | 0.1997 | 0 | 9 | 28 | 0.0169 | 0.0599 | 0.0065 |
| 16 | 17 | 0.0524 | 0.1923 | 0 | | ı | <u>I</u> | | 1 |

BCAP *= half total line charging susceptance

Table 6.4 Bus Data for 30-Bus system

| Bus no | Voltage sche- dule(pu | P _{gen} (pu MW) | P _{load} (pu MW) | Q _{load} (pu MVAR) | Bus no | Voltage sche- dule(pu | P _{gen} (pu MW) | P _{load} (pu MW) | Q _{load} (pu MVAR) |
|--------|-----------------------------|--------------------------|---------------------------------|-----------------------------|--------|-----------------------------|--------------------------|---------------------------------|-----------------------------------|
| | V) | 141 44) | 141 44) | WI V / KIK) | | V) | 141 44) | 1 | |
| 1 | 1.060 | 0 | 0 | 0 | 16 | 1.0 | 0 | 0.035 | 0.018 |
| 2 | 1.043 | 0.4 | 0.217 | 0.127 | 17 | 1.0 | 0 | 0.090 | 0.058 |
| 3 | 1.010 | 0.2 | 0 | 0.300 | 18 | 1.0 | 0 | 0.032 | 0.009 |
| 4 | 1.010 | 0 | 0.300 | 0 | 19 | 1.0 | 0 | 0.095 | 0.034 |
| 5 | 1.082 | 0 | 0.942 | 0.190 | 20 | 1.0 | 0 | 0.022 | 0.007 |
| 6 | 1.071 | 0 | 0 | 0 | 21 | 1.0 | 0 | 0.175 | 0.112 |
| 7 | 1.0 | 0 | 0 | 0 | 22 | 1.0 | 0 | 0 | 0 |
| 8 | 1.0 | 0 | 0.058 | 0.020 | 23 | 1.0 | 0 | 0.032 | 0.016 |
| 9 | 1.0 | 0 | 0.112 | 0.075 | 24 | 1.0 | 0 | 0.087 | 0.067 |
| 10 | 1.0 | 0 | 0 | 0 | 25 | 1.0 | 0 | 0 | 0 |
| 11 | 1.0 | 0 | 0.076 | 0.016 | 26 | 1.0 | 0 | 0.035 | 0.023 |
| 12 | 1.0 | 0 | 0.228 | 0.109 | 27 | 1.0 | 0 | 0.024 | 0 |
| 13 | 1.0 | 0 | 0 | 0 | 28 | 1.0 | 0 | 0 | 0 |
| 14 | 1.0 | 0 | 0.062 | 0.016 | 29 | 1.0 | 0 | 0.024 | 0.009 |
| 15 | 1.0 | 0 | 0.082 | 0.025 | 30 | 1.0 | 0 | 0.106 | 0.019 |

Bus no:1- Slack bus, Bus no: 2,3,4,5,6-Generator bus, Rest all are Load busses